





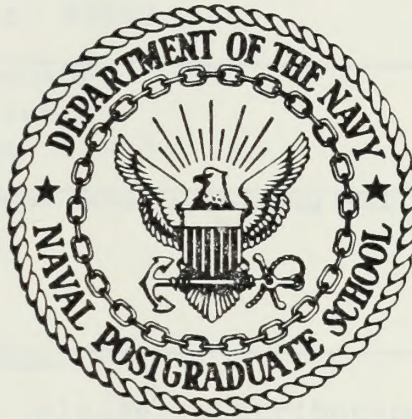
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# NAVAL POSTGRADUATE SCHOOL

## Monterey, California



# THESIS

PRELIMINARY HELICOPTER DESIGN DECISION  
MAKING BASED ON FLIGHT PERFORMANCE FACTORS

by

Patrick V. Adamcik

September 1984

Thesis Advisor:

Donald M. Layton

Approved for public release: Distribution unlimited

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## 20. continuation

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Preliminary Helicopter Design Decision Making Based  
on Flight Performance Factors

by

Patrick V. Adamcik  
Captain, United States Army  
B.S., University of Texas at Austin, 1977

Submitted in partial fulfillment of the  
requirements for the degree of

MASTER OF SCIENCE IN AERONAUTICAL ENGINEERING

from the

NAVAL POSTGRADUATE SCHOOL  
September 1984

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ABSTRACT

This thesis will assist those evaluating helicopter design to make preliminary judgments about the feasibility of new designs. By using the computer program developed in this thesis, a designer can produce estimates for power requirements, endurance velocity, rate of climb, range velocity, hover ceiling, and service ceiling versus main rotor radius. These estimates can also be examined for the effects of changes in main rotor radius, chord, and rotational velocity.



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## I. INTRODUCTION

A military engineering officer in a program or project office would probably never be called on to prepare a conceptual design of a helicopter, but he may well be required to evaluate a proposal submitted by a commercial contractor.

The requirement for such an evaluation might be stated as:

Determine if this design meets or exceeds the performance factors listed on the next page and if the design can be changed to optimize the performance.

There are several approaches one could use to complete this task. One could use a hand held calculator and enter the data for the many equations, or one could write a program for a micro or main frame computer to produce the required information. Both these options are laborious and time-consuming. By choosing the first option, one may be able to complete the task in two or three weeks or if it is decided to write a program, one may finish in one week provided that there are no "bugs".

The best solution of course, is to use an existing program which can determine the necessary information for the specification parameters. In addition, this program should be able to show what happens if certain parameters

are allowed to vary, thus providing the formation for optimization.

The objective of this thesis was to develop such a program that will graphically represent power requirements, endurance velocity, rate of climb, range velocity, hover ceiling and service ceiling all as a function of main rotor radius for four different cases. The graphs that result from this program should enable one not only to evaluate the basic helicopter design, but also to make recommendations for design improvement.



## II. APPROACH TO THE PROBLEM

Six performance factors (power requirements, endurance velocity, rate of climb, range velocity, hover ceiling and service ceiling) were determined to be major in designing of a helicopter. In order to obtain estimates for these, a Fortran program was to be written to be used with "DISSPLA" (Display Integrated Software System and Plotting Language), [Ref. 1], to plot the results of the performance factors versus main rotor radius on either a screen or as a hard copy from the main frame computer.

The equations required for calculating these factors were obtained from "Helicopter Performance", [Ref. 2], and "Helicopter Design Manual", [Ref. 3], both written by Donald M. Layton. These equations were examined and then grouped for the purpose of writing subroutines to ensure an effective use of computer time. The result was six subroutines, Sub-group A, [Appendix B], are used in all the performance calculations. Sub-group A consist of:

1. RHO - Calculates density from pressure altitude and temperature or given density altitude. Also determines pressure and temperature ratio for altitude versus sea level.
2. VELMR - Calculates induced velocity for main rotor.
3. VELTR - Calculates induced velocity for tail rotor.

4. POWMR - Calculates power requirements for main rotor only.

5. POWTR - Calculates power requirements for tail rotor and total aircraft.

6. CONST - Calculates general constants to be used in the first five subroutines listed above.

In addition to the subroutines listed above, six more, Sub-group B, [Appendix B], were written to perform the necessary iterations to calculate the performance factors. Some of Sub-group B subroutines were iterated in steps (1000,100,10,1) so that it would not require extensive computer time to obtain the desired results. A final eight subroutines, Sub-group C, [Appendix B], were written to plot the results using DISPLA.

The program takes into account neither compressibility nor blade stall. These considerations were omitted since this program was aimed at facilitating preliminary decision making for a new design, rather than a final production design, and usually the blade selected for a new design is taken from an existing helicopter.

### III. SOLUTION TO THE PROBLEM

The program requires input data prior to compiling and execution. To demonstrate how to use the program a set of sample data was used. Table 1 is a listing of the required input data for the program.

Table 1

#### Sample Data for Use in Program

	Main Rotor	Tail Rotor
Radius	26.8 ft	5.5 ft
Chord	1.75 ft	0.81 ft
Rotational velocity	27.0 rad/sec	124.6 rad/sec
Coefficient of drag	0.008	0.008
Number of blades	4	4

#### General Helicopter Data

Weight	20000.0 lbs
Tail boom length	31.5 ft
Effective flat plate area (forward)	25.7 sq ft
Effective flat plate area (vertical)	31.8 sq ft
Main rotor height above skids or wheels	11.2 ft
Aircraft velocity (power calculations only)	90.0 kts
Plus/minus (+/-) value for main rotor radius	4.0 ft

#### Engine Data

Number of engines	2
Shaft horsepower output (military)	1561.0 shp
Shaft horsepower output (normal)	1318.0 shp
Shaft horsepower output (cruise)	989.0 shp
Specific fuel consumption (military)	0.46 lbs/shp/hr
Specific fuel consumption (normal)	0.47 lbs/shp/hr
Specific fuel consumption (cruise)	0.51 lbs/shp/hr

As indicated in Table 1, a value is inputted for the range over which you wish to examine the main rotor radius.



The example uses a value of four (4.0) feet. This value is assigned to a variable called "diff". The program was written to allow the X-axis scale of the plot to be adjusted in accordance with any value you might choose for "diff". The Y-axis scales can also change based on the maximum and minimum values for the performance factor being considered.

Certain assumptions had to be made in order to write the program. Table 2 lists these assumptions and factors used and the line number in the program where the factors can be changed if needed.

Table 2  
Assumptions Made in the Program

Assumption	Factor	Line Number
Single Mast Helicopters	NA	NA
Only Rectangular Blades	NA	NA
Profile Power Factor	4.3	1079,1108
Ground Effect Factor	1.6	1138
Transmission & Accessory Losses		
1 engine SHP = (# ENG*ESHP-10.0)*0.97		560,780.887
2 engines SHP = (# ENG*ESHP-10.0)*0.9*0.97		561,781.888
3 engines SHP = (# ENG*ESHP-10.0)*0.9*0.94		562,782.889

ENG: Engine, ESHP: Engine shaft horsepower,  
SHP: Rotor Shaft horsepower

The Transmission and Accessory Losses were calculated based on a loss of ten (10) horsepower for the accessories, ten percent (10%) for multiple engine installation, and three

percent (3%) for transmission losses (if three engines are used, an additional transmission is required), [Ref. 2].

The secondary goal of the thesis was to examine four (4) different cases involving main rotor Radius, Chord, Rotational Velocity, Tip Velocity, Advance Ratio, and Solidity. Table 3 shows how these variables were used in each of the four (4) cases.

Table 3

Case Use of Variables

	Radius	Chord	Rotational Velocity	Advance Ratio	Tip Velocity	Solidity
Case 1	V	C	C	V	V	V
Case 2	V	C	V	C	C	V
Case 3	V	V	C	V	V	C
Case 4	V	V	V	C	C	C

V : VARIES      C : HELD CONSTANT

Advance Ratio, Tip Velocity, and Solidity when held constant keep their values at the specification conditions. The values of Chord and Rotational Velocity were allowed to vary when Advance Ratio, Tip Velocity, or Solidity were held constant as shown in Table 3.

The graphs consist of two (2) plots representing the same data but presented in different ways. The left hand plot shows the actual performance factor value versus main rotor radius. Figure 3.1 shows an example using power required versus main rotor radius, Case 1.

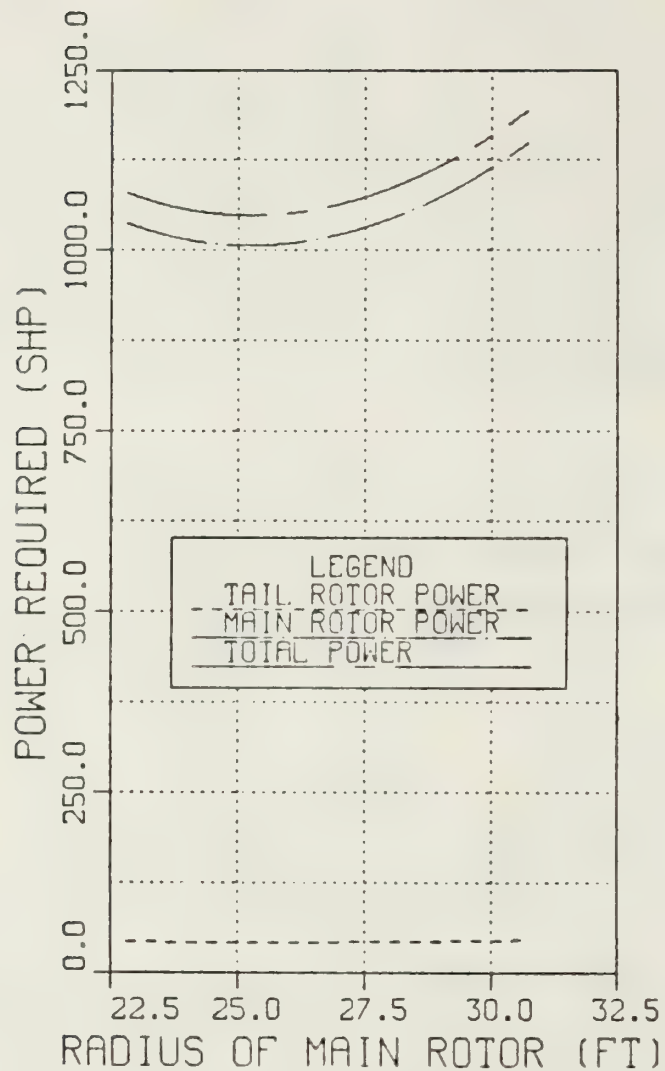


Figure 3.1 Example of Left Hand Plot

The right hand plot shows the values of the performance factors based on a percent difference from the value at the specification conditions versus a percent difference of the radius from the radius specification. Figure 3.2 shows an example of power required (% change) versus radius of the main rotor (% change), Case 1.



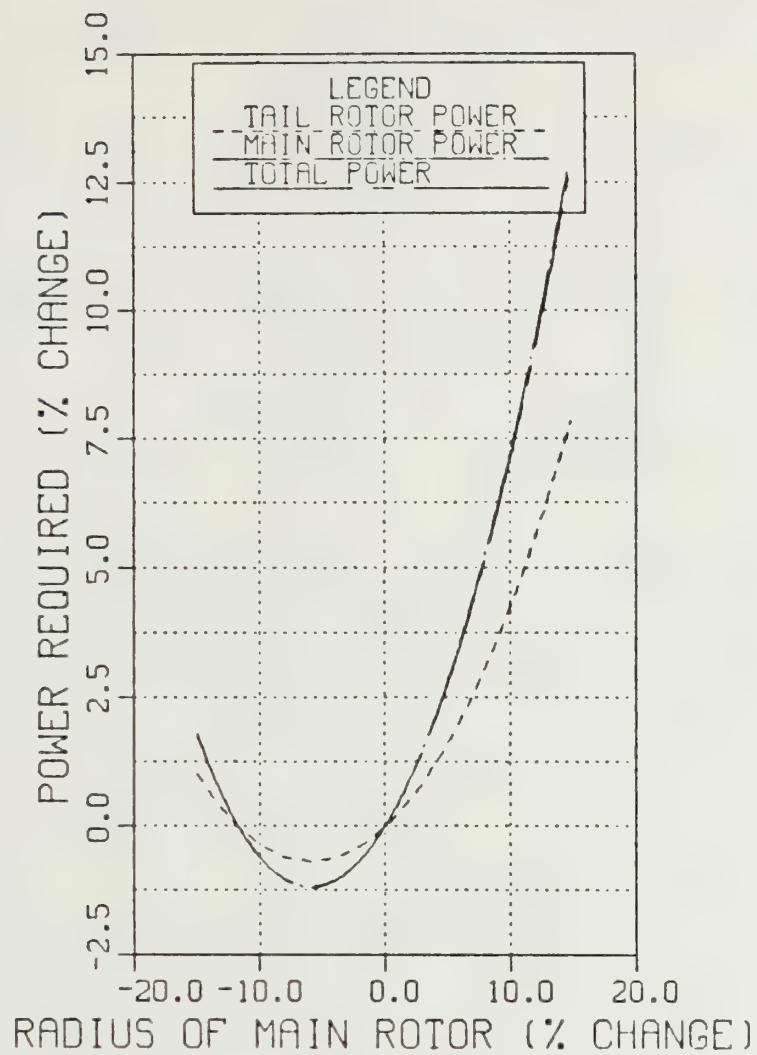


Figure 3.2 Example of Right Hand Plot

#### IV. RESULTS

The program will generate a total of thirty two (32) plots. The first twelve (12) pertain to power requirements. This includes induced, profile, and parasite power for the main rotor; and induced and profile power for the tail rotor. To indicate a relation between the power terms of the main rotor the figure of merit (induced divided by the sum of the induced and profile power) is included. The sum of the terms (total power) for the main and tail rotor was included with the total power required for the aircraft. The remaining twenty (20) plots are for the performance factors of endurance velocity, rate of climb, range velocity, hover ceiling and service ceiling.

The data for this particular model (UH-60A) was used to illustrate the features of the program and the results presented are typical for this example only. The specifications of any model or design can be used as long as the assumption of a single-mast helicopter with rectangular blades is followed.

The plots created by the program represent the results of varying the main rotor radius, chord or rotational velocity. To example how to interrupt the results, the four (4) plots for Maximum Rate of Climb will be analyzed. Table 4 compares the results in relation to rate of climb, radius

and percent increase of rate of climb. The cases were explained in Table 3 and the Figures follow Table 4.

Table 4

Case Evaluation of Maximum Rate of Climb Plots

Case	Figure Reference	Rate of Climb(ft/sec)	Radius (ft)	Percent Increase
1	4.1	2628	27.8	+ 0.130
2	4.2	2668	24.8	- 0.156
3	4.3	2700	30.63	+ 2.80
4	4.4	2637	25.63	- 5.00

From examining Table 4, it would be best to increase the radius to 30.63 feet while holding the chord to 1.75 feet. the tip velocity to 723.6 ft/sec (radius times rotational velocity), changing the rotational velocity to 23.62 rad/sec, and calculating solidity from radius and chord. This, however, may not be the best answer if there is a limitation to the radius of the blade. For this particular example, the optimum solution may be to leave the design as it is. Increasing or decreasing the radius by small amounts does little to increase or decrease the rate of climb.

One must not only look at one factor in making the final decision. The changes affect the performance factors in different ways, therefore, the final decision must be made after weighting all the changes against all the performance factors.



MAXIMUM RATE OF CLIMB VERSUS RADIUS CHANGE  
 CHORD & ROTATIONAL VELOCITY HELD CONSTANT  
 SOLIDITY, TIP VELOCITY & ADVANCE RATIO  
 ALLOWED TO VARY WITH RADIUS

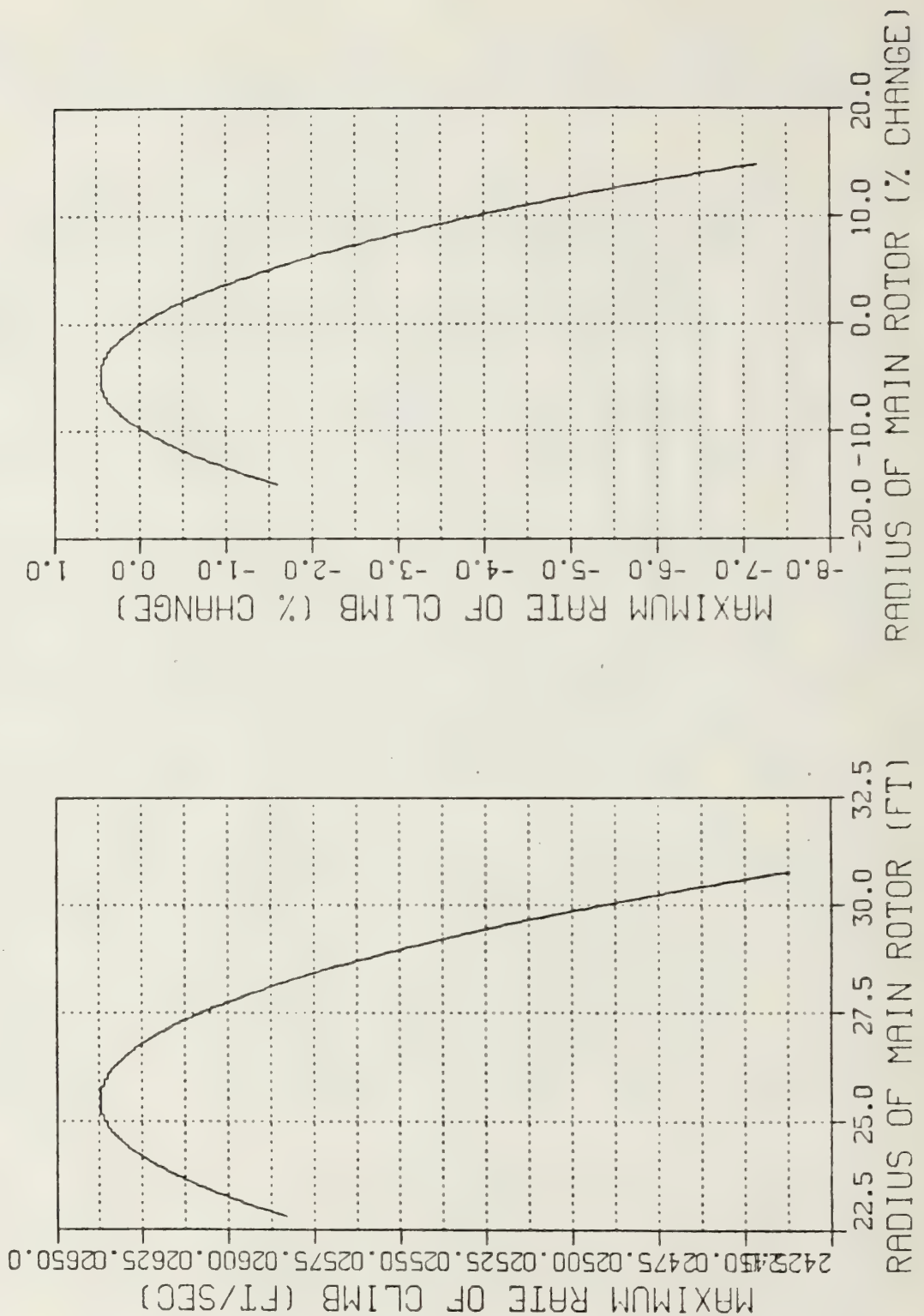


Figure 4.1 Example Maximum Rate of Climb - Case 1

# MAXIMUM RATE OF CLIMB VERSUS RADIUS CHANGE CHORD, TIP VELOCITY & ADVANCE RATIO HELD CONSTANT SOLIDITY, ROTATIONAL VELOCITY ALLOWED TO VARY WITH RADIUS

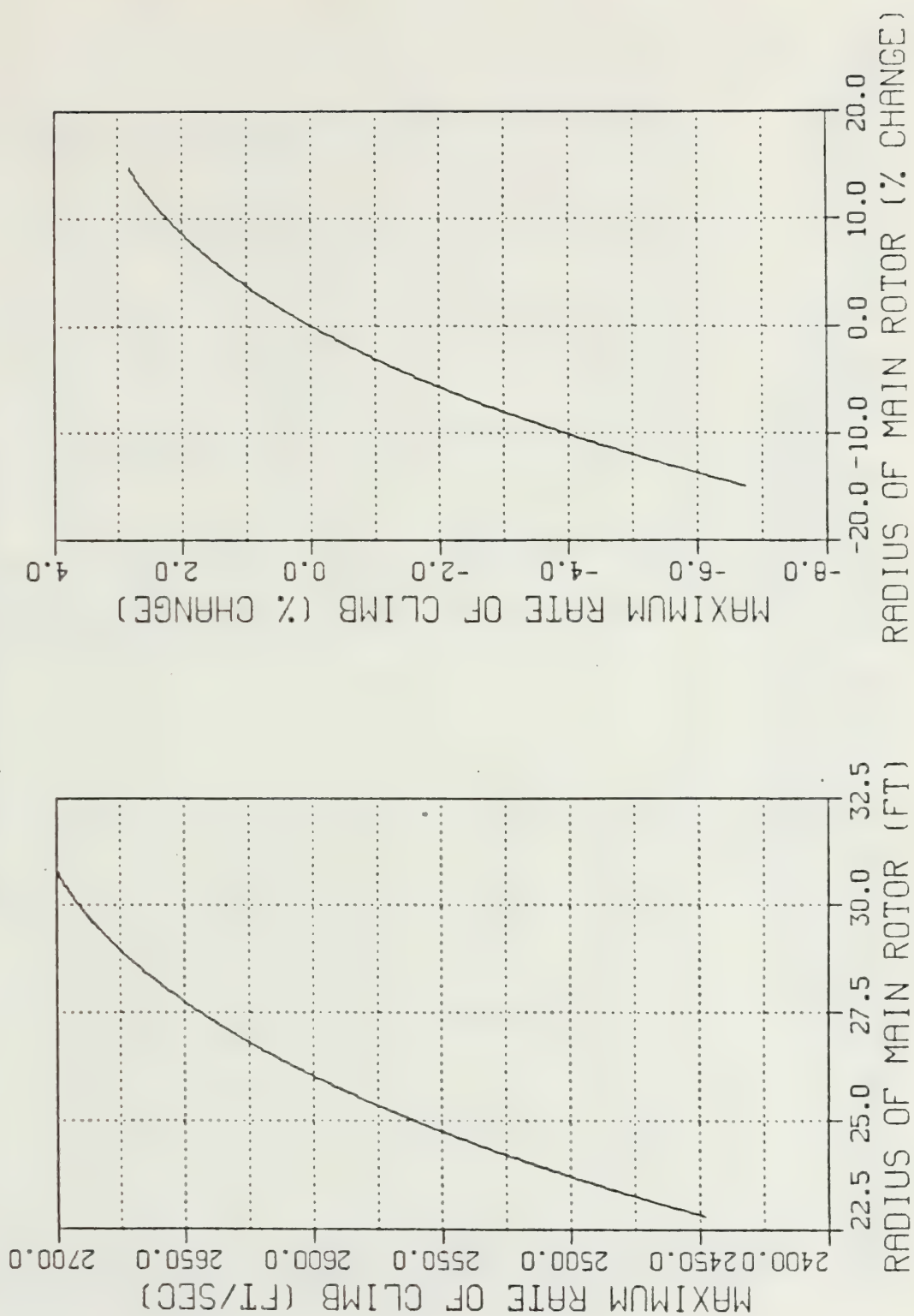


Figure 4.2 Example Maximum Rate of Climb - Case 2

MAXIMUM RATE OF CLIMB VERSUS RADIUS CHANGE  
 SOLIDITY & ROTATIONAL VELOCITY HELD CONSTANT  
 CHORD, ADVANCE RATIO & TIP VELOCITY  
 ALLOWED TO VARY WITH RADIUS

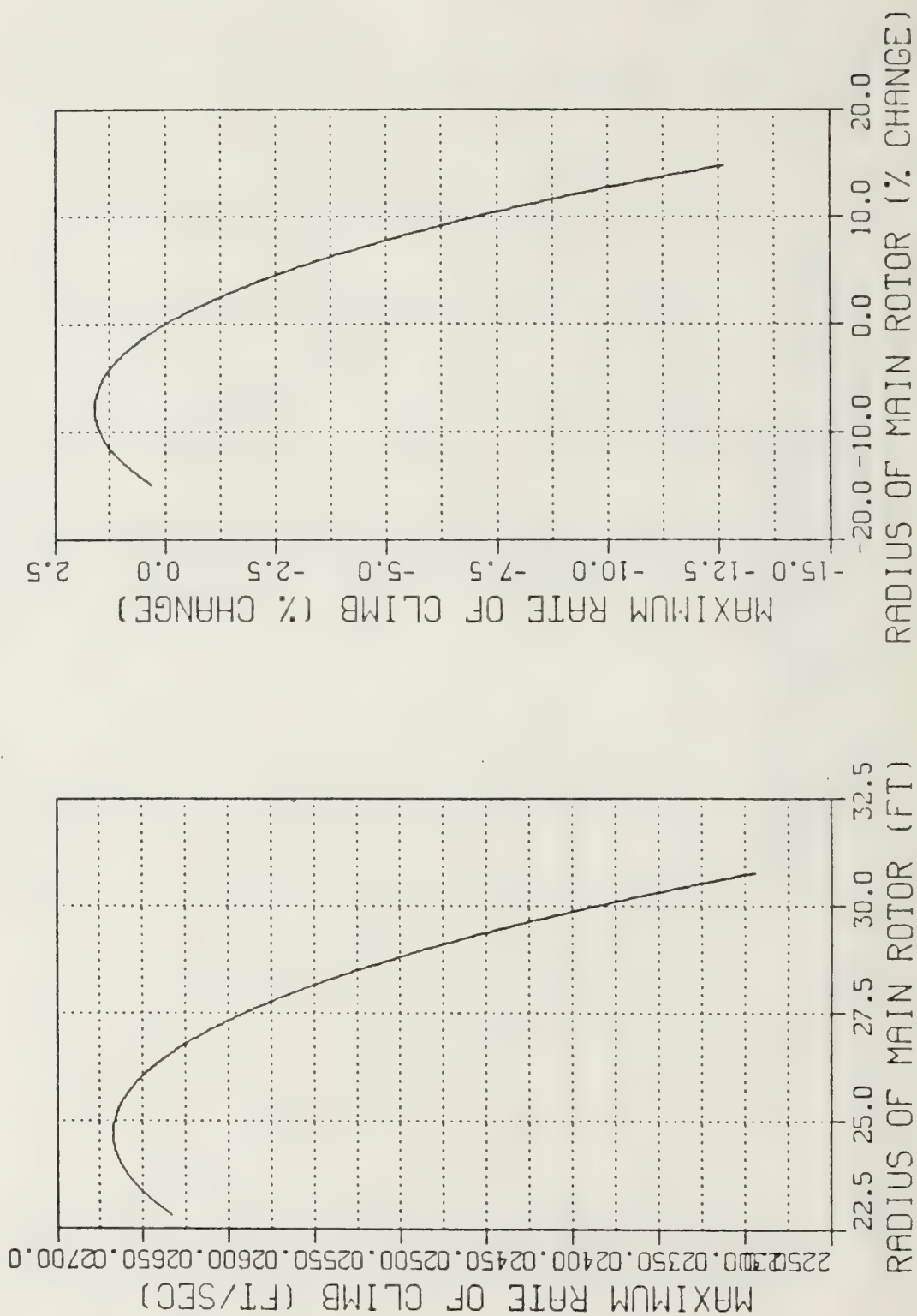


Figure 4.3 Example Maximum Rate of Climb - Case 3



# MAXIMUM RATE OF CLIMB VERSUS RADIUS CHANGE SOLIDITY, ADVANCE RATIO & TIP VELOCITY HELD CONSTANT CHORD & ROTATIONAL VELOCITY ALLOWED TO VARY WITH RADIUS

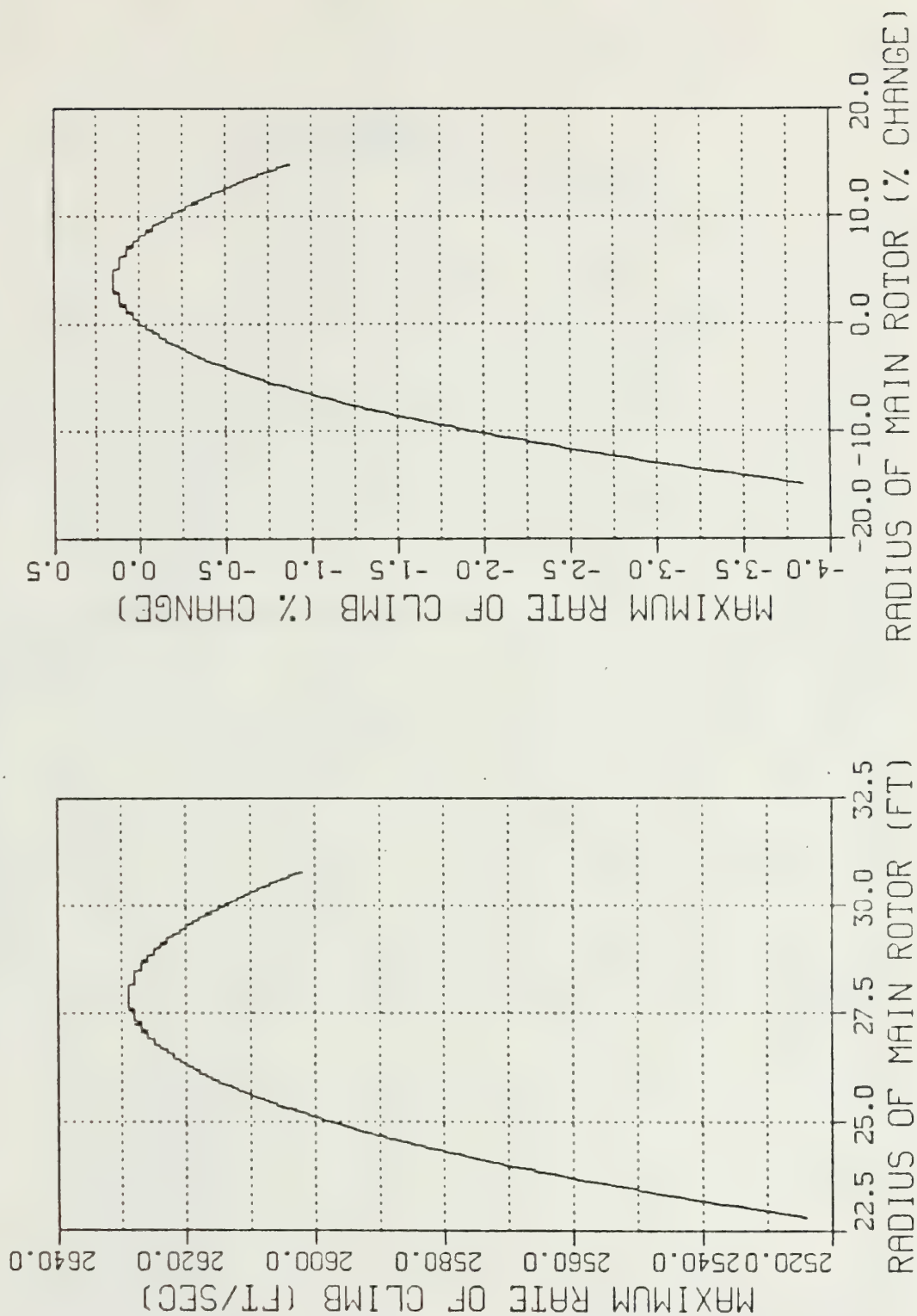


Figure 4.4 Example Maximum Rate of Climb - Case 4

## V. CONCLUSIONS

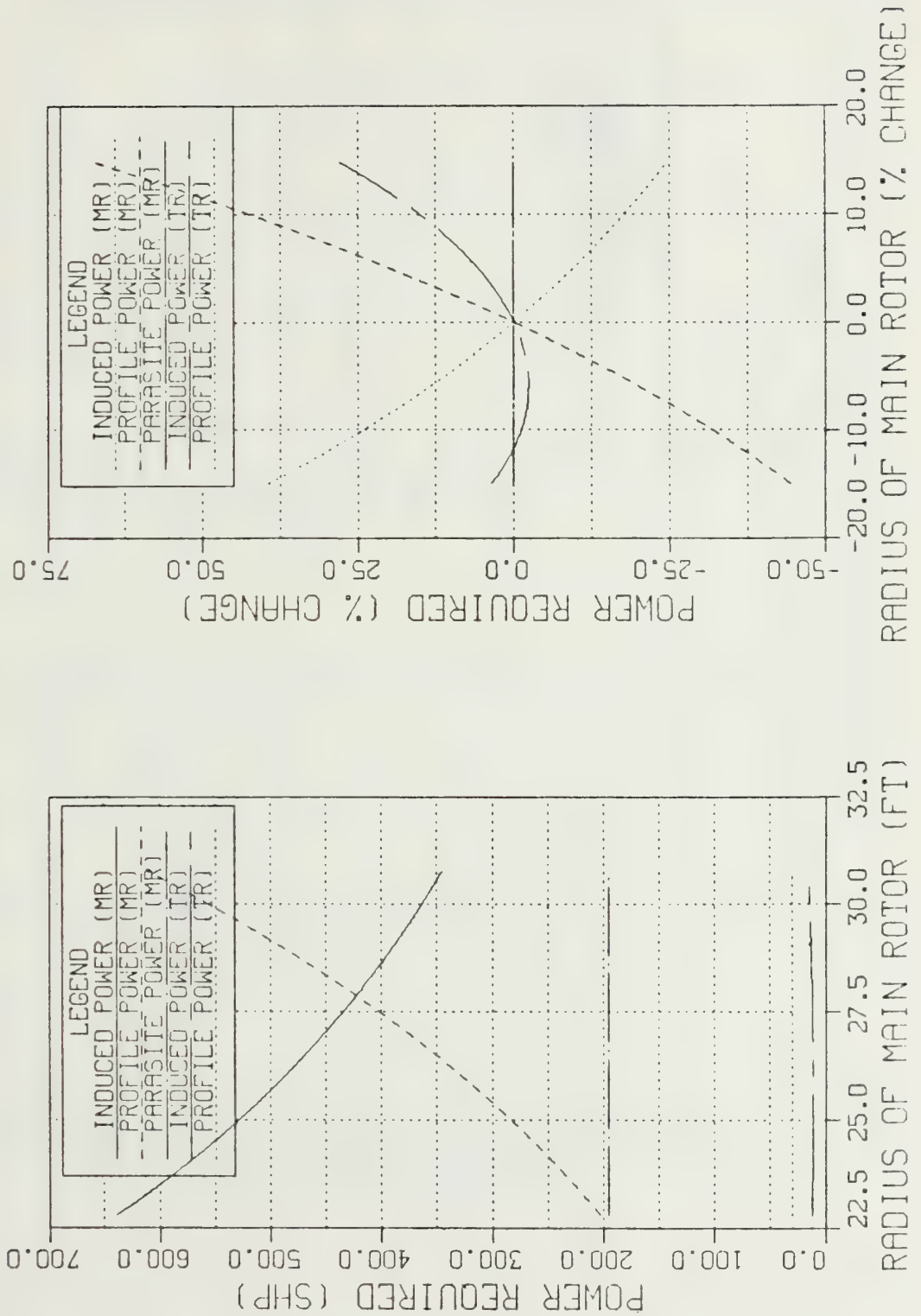
The objective of this thesis to design a program that evaluates a given set of helicopter design values was accomplished. The program will generate thirty two (32) graphs of six (6) performance factors for any single-mast helicopter. The program does allow for one to optimize a design through the evaluation of the variation of parameters for each performance factor.

At this point, the program takes into account neither compressibility nor blade stall. These factors would improve the estimations and may prove to be a worthwhile project for further work. Other points which could be examined are twin-blade and no-tail-rotor helicopters. Of the points mentioned above, blade design would probably be of most importance since little has been done to examine the optimization of blade twist and composite structure of blades.

# POWER VERSUS RADIUS CHORD & ROTATIONAL VELOCITY HELD CONSTANT SOLIDITY, TIP VELOCITY & ADVANCE RATIO ALLOWED TO VARY WITH RADIUS

## APPENDIX A

### COMPUTER PROGRAM OUTPUT - PLOTS



# POWER VERSUS RADIUS CHORD & ROTATIONAL VELOCITY HELD CONSTANT SOLIDITY, TIP VELOCITY & ADVANCE RATIO ALLOWED TO VARY WITH RADIUS

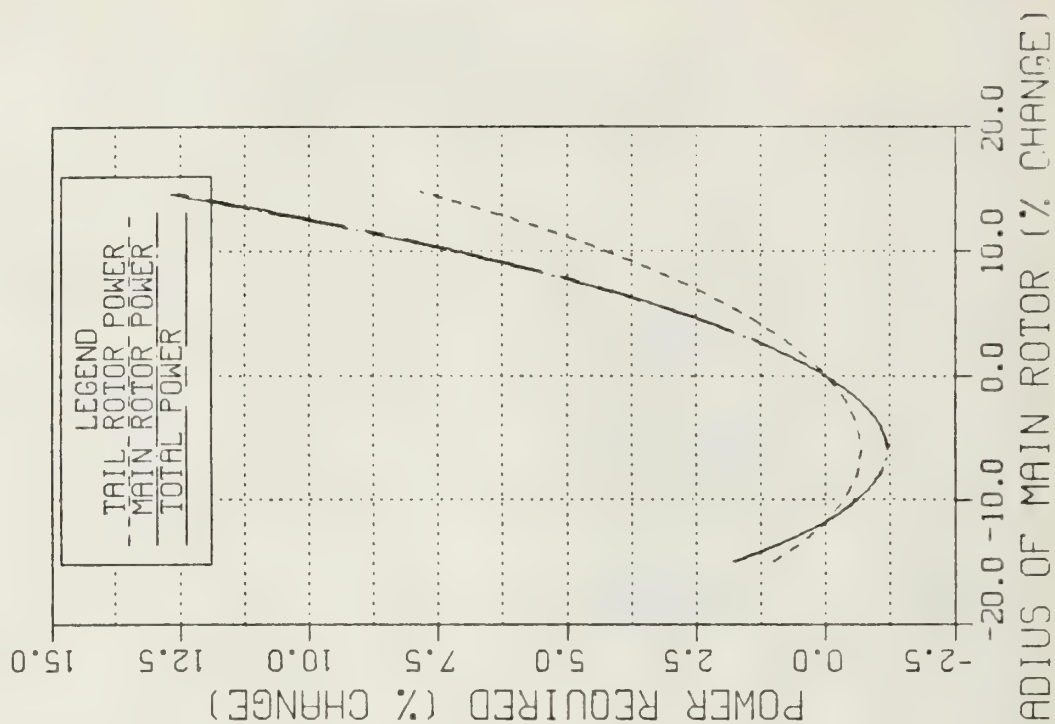
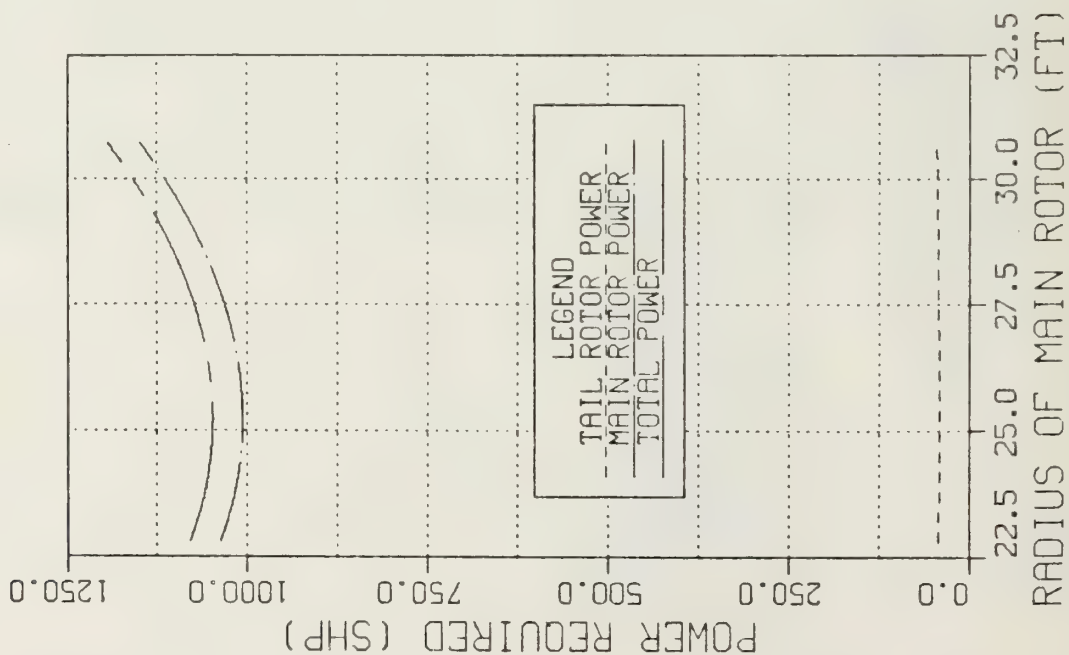
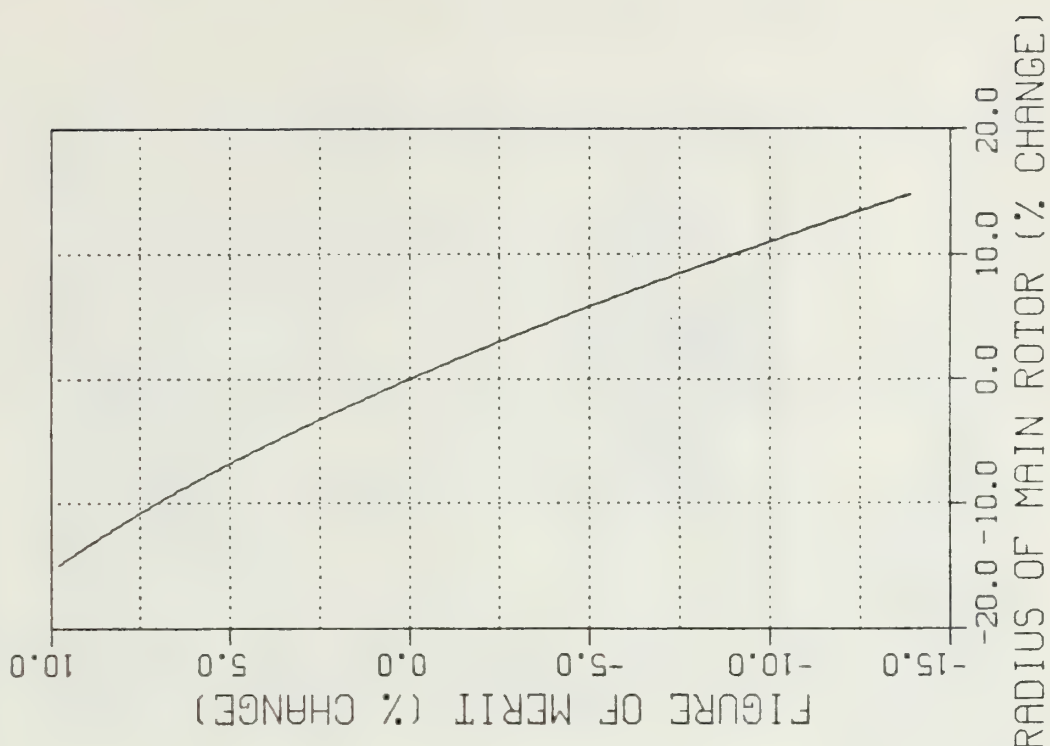
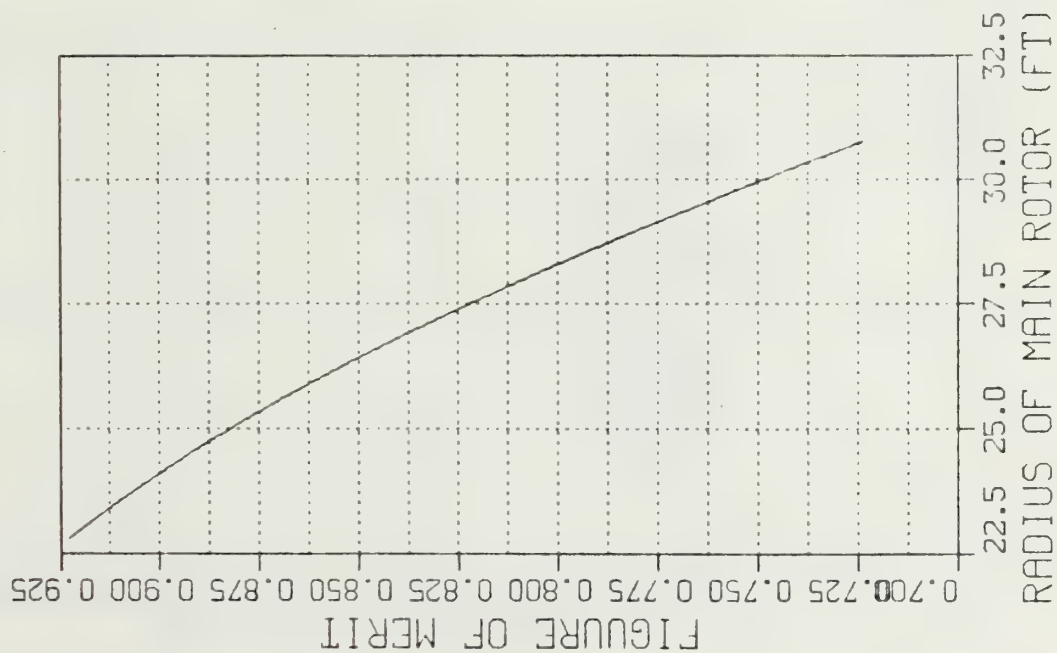
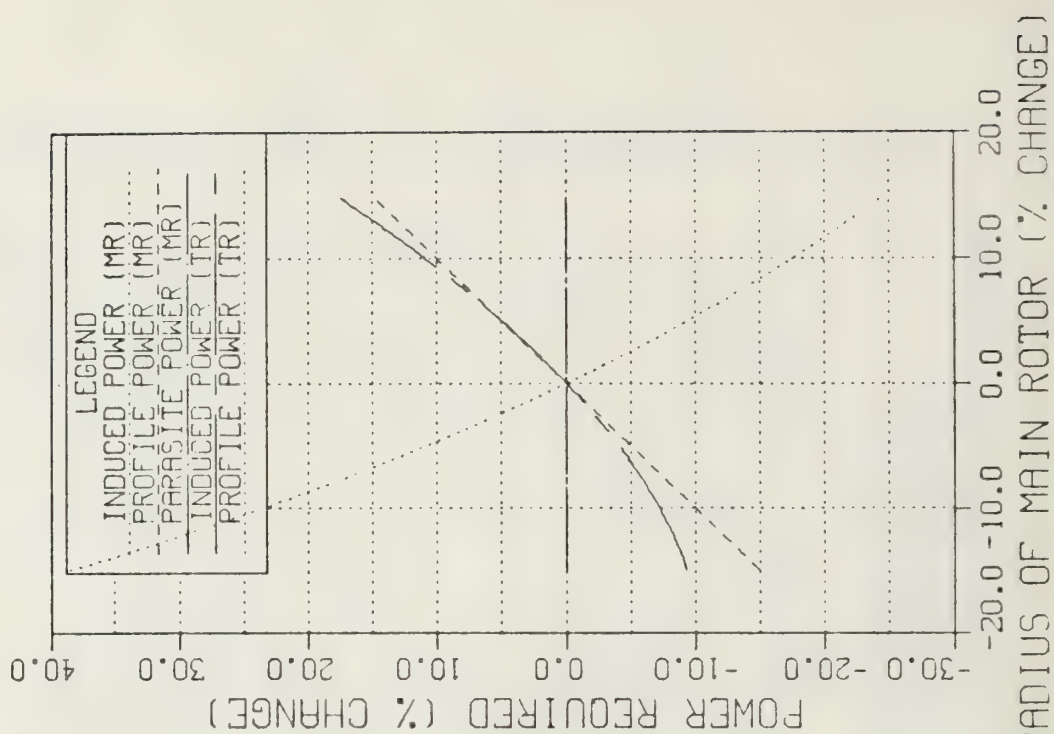
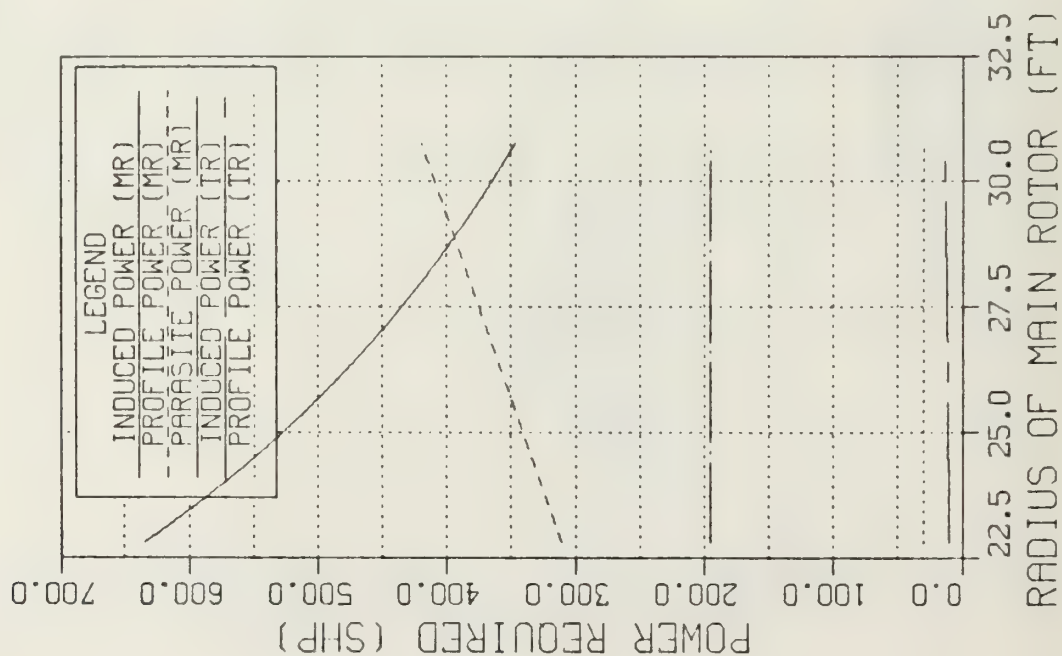




FIGURE OF MERIT VERSUS RADIUS CHANGE  
 CHORD & ROTATIONAL VELOCITY HELD CONSTANT  
 SOLIDITY, TIP VELOCITY & ADVANCE RATIO  
 ALLOWED TO VARY WITH RADIUS



# POWER VERSUS RADIUS CHORD, TIP VELOCITY & ADVANCE RATIO HELD CONSTANT SOLIDITY, ROTATIONAL VELOCITY ALLOWED TO VARY WITH RADIUS



# POWER VERSUS RADIUS

CHORD, TIP VELOCITY & ADVANCE RATIO HELD CONSTANT  
SOLIDITY, ROTATIONAL VELOCITY  
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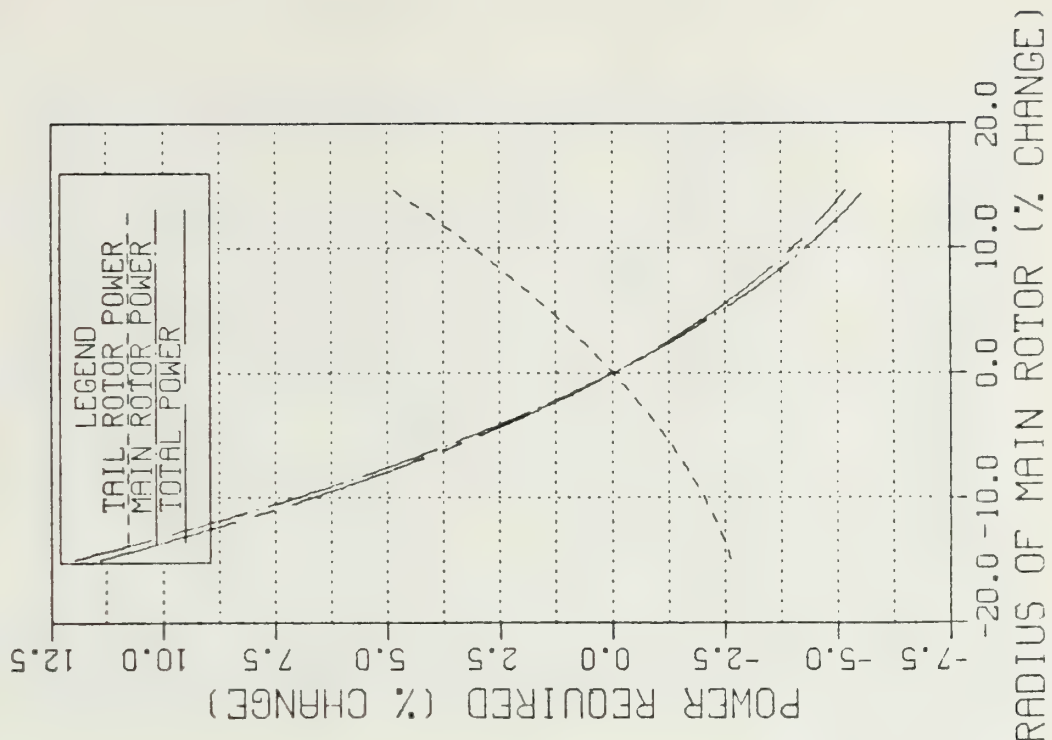
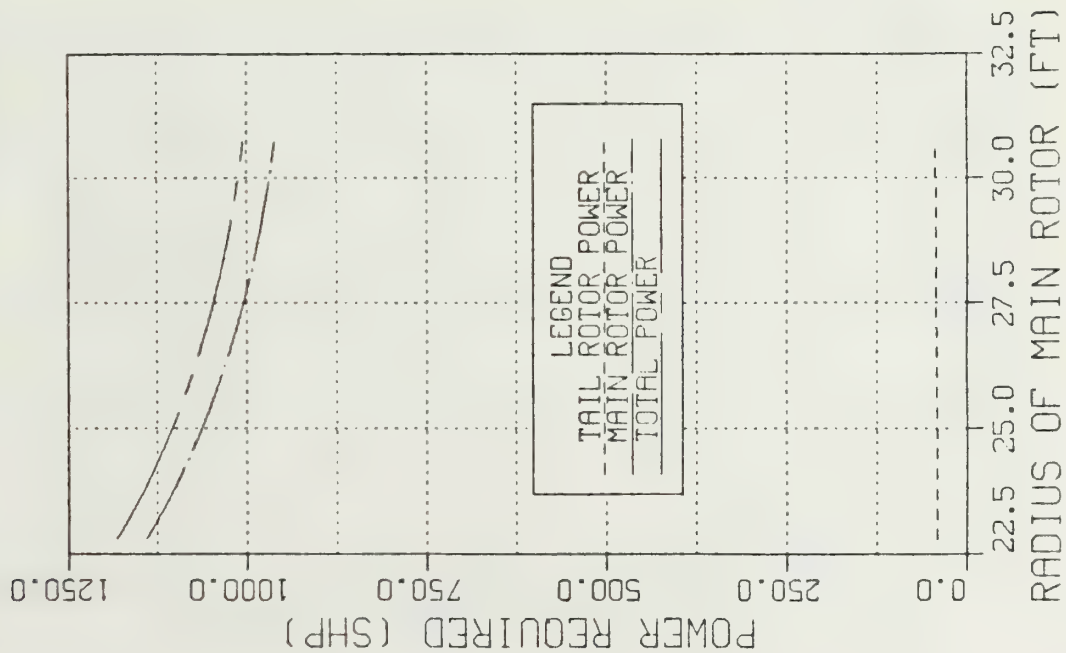
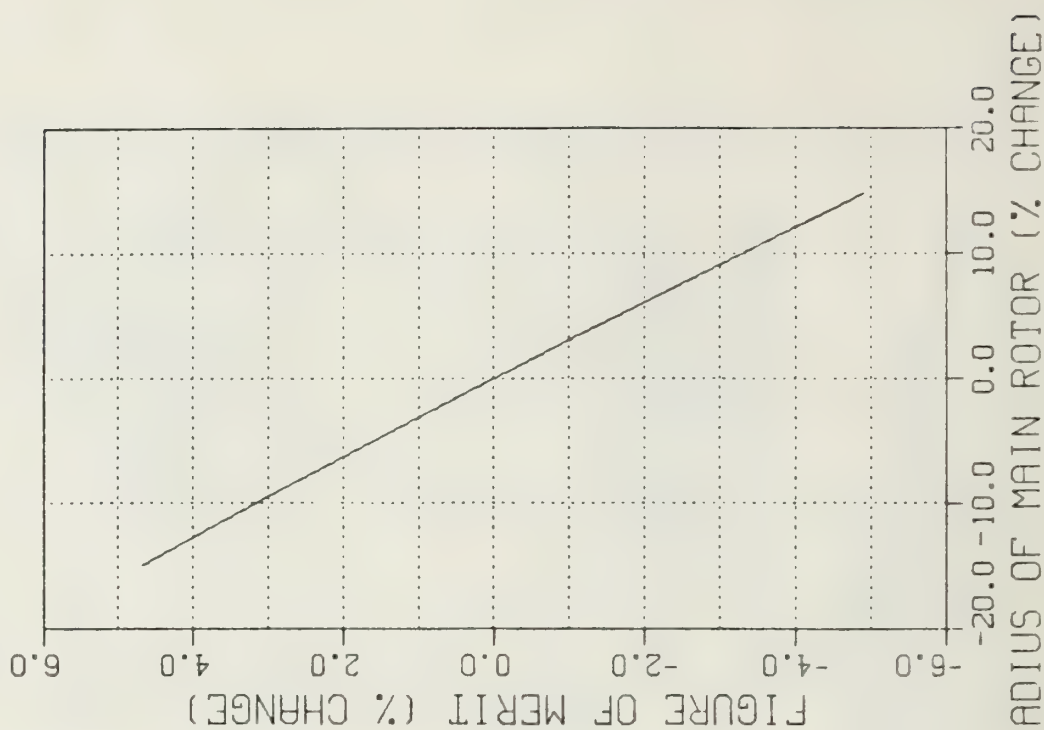
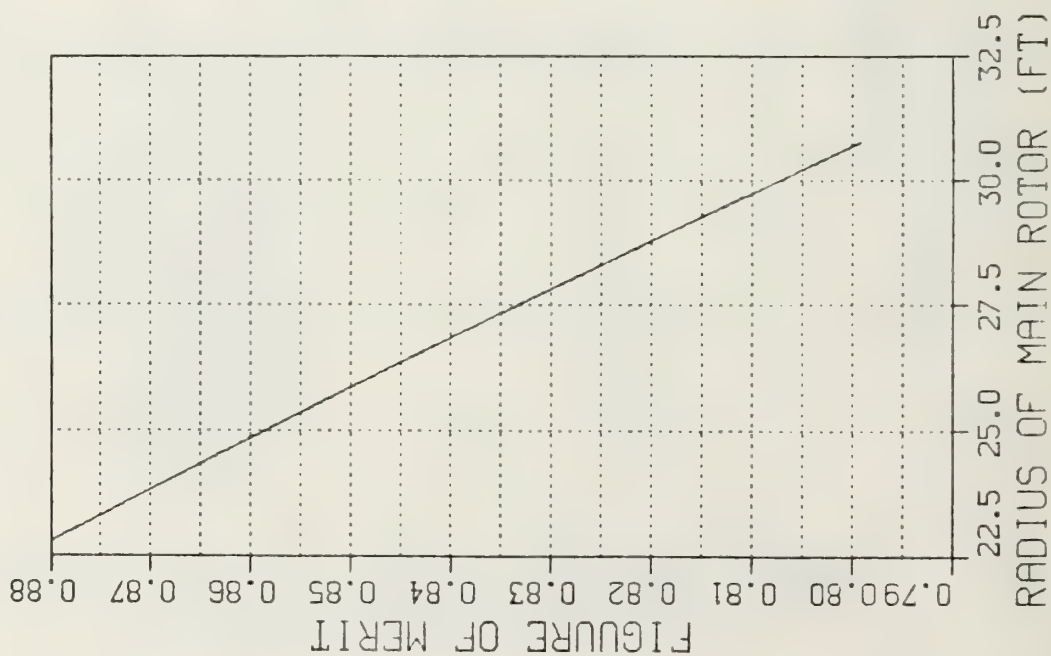
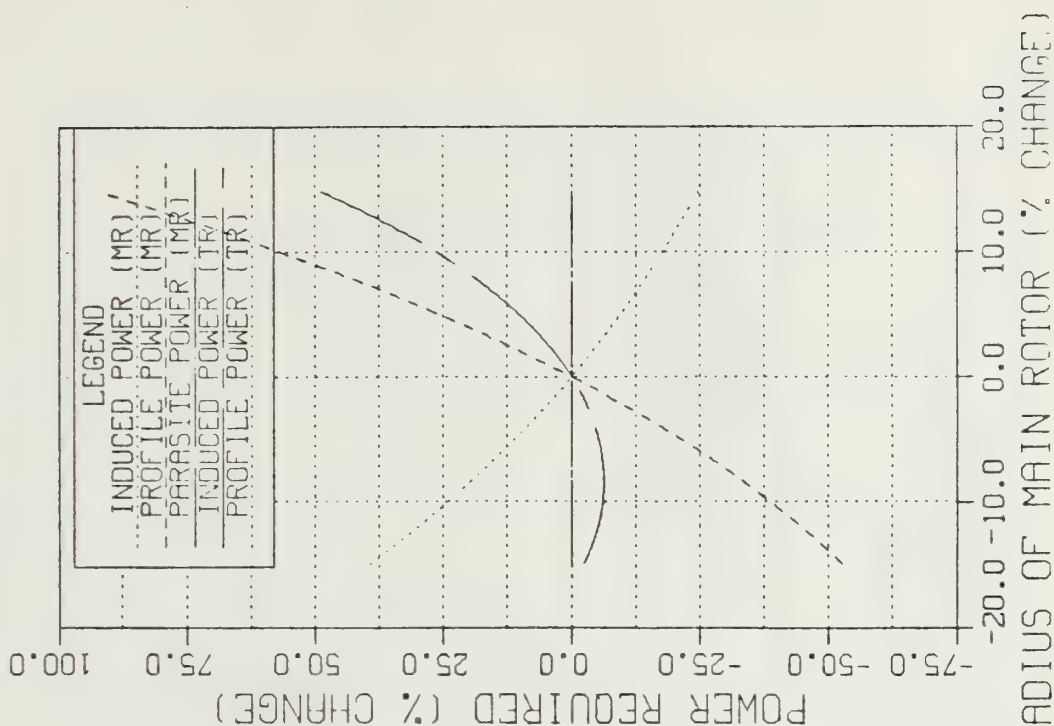
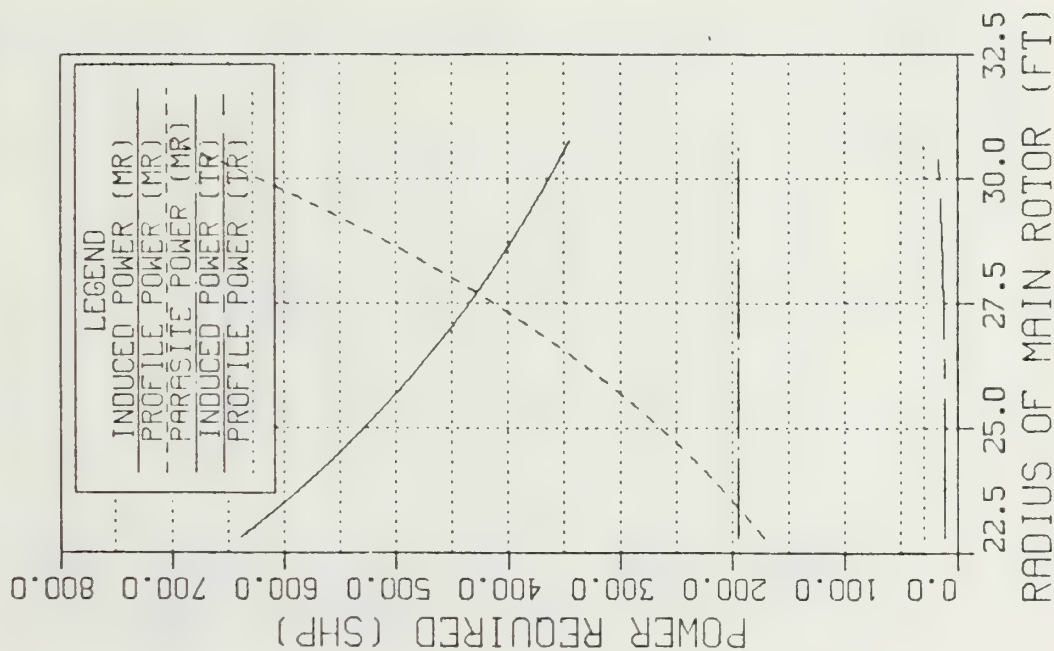


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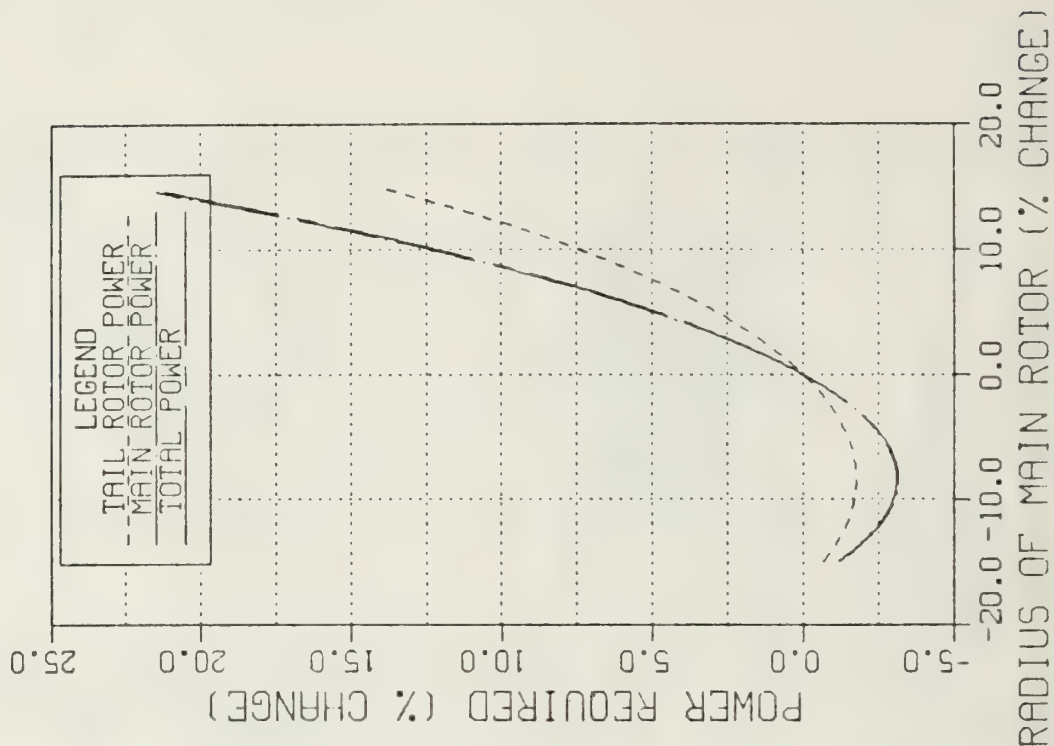
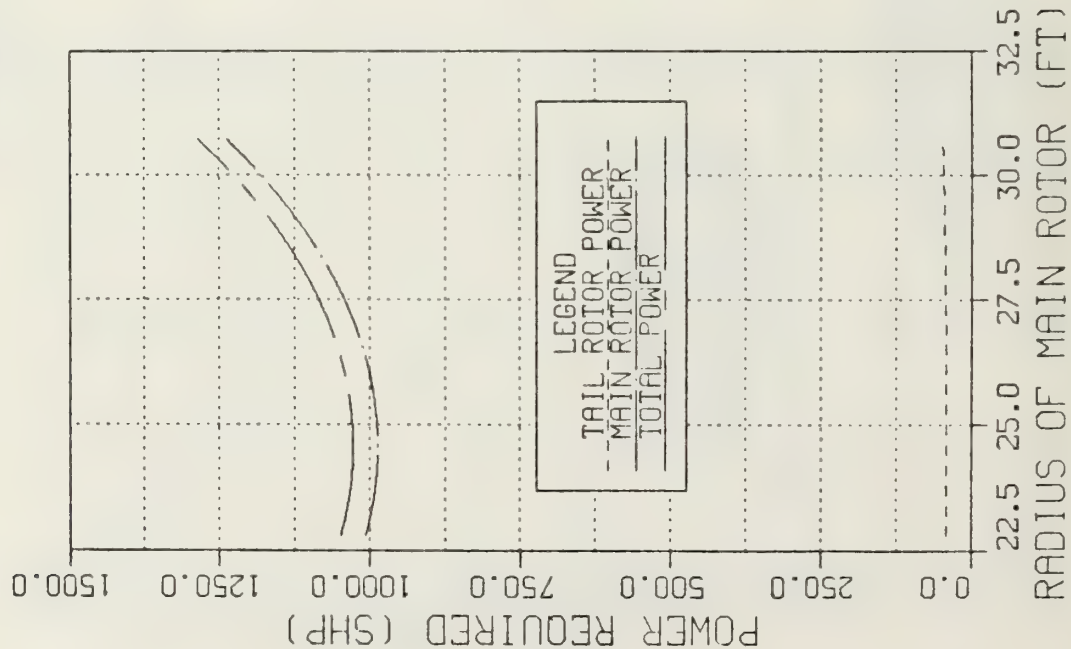




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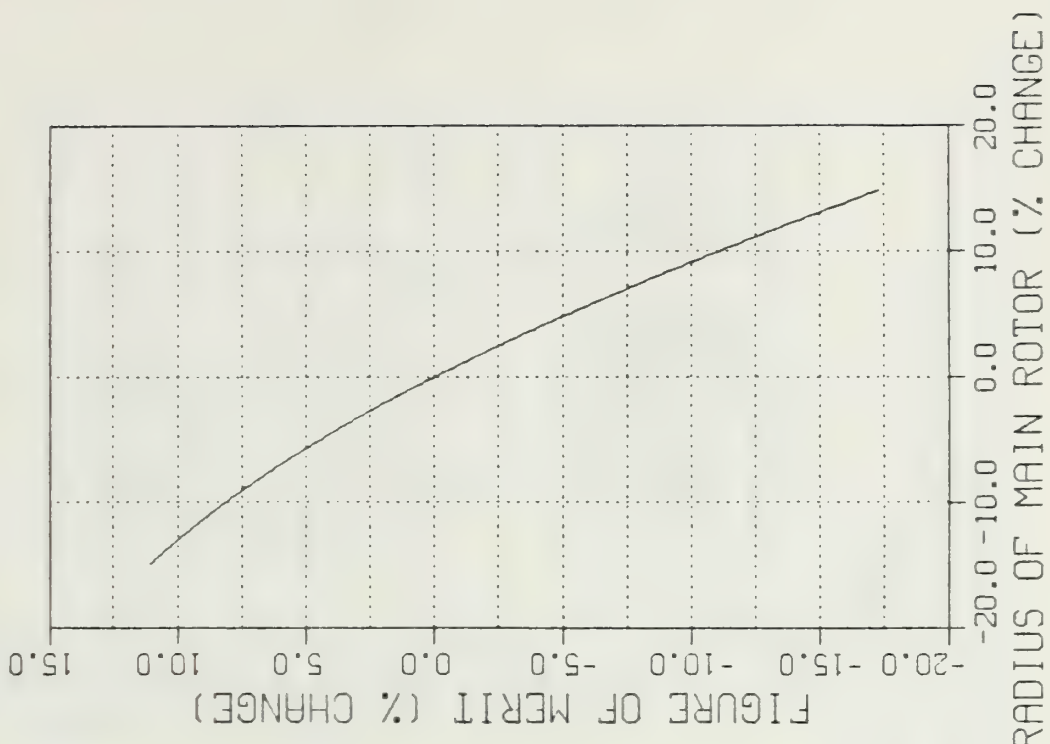
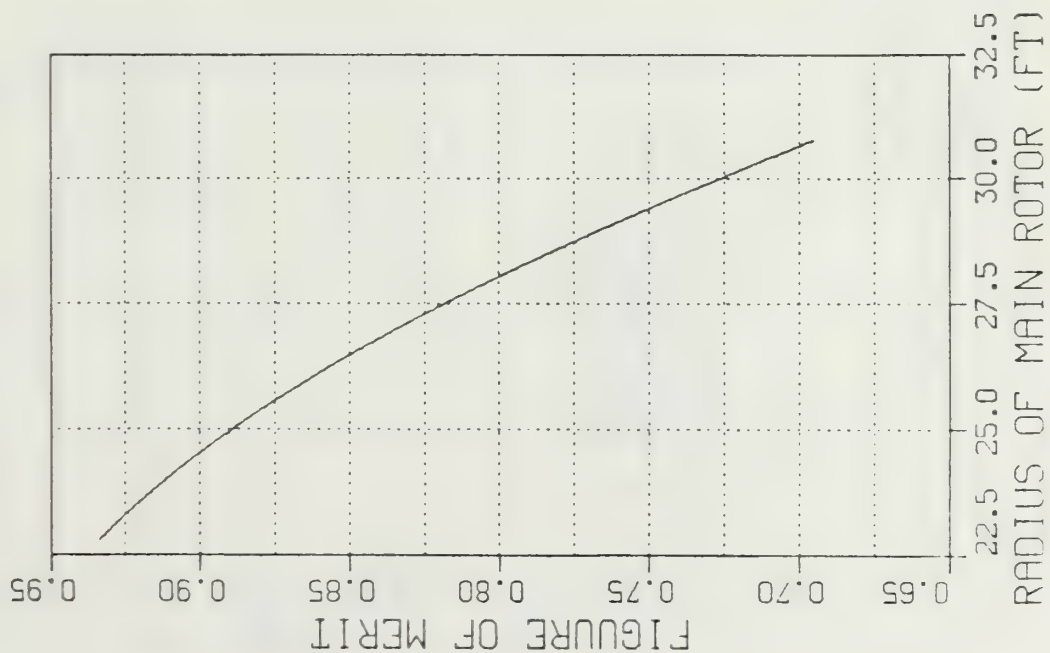


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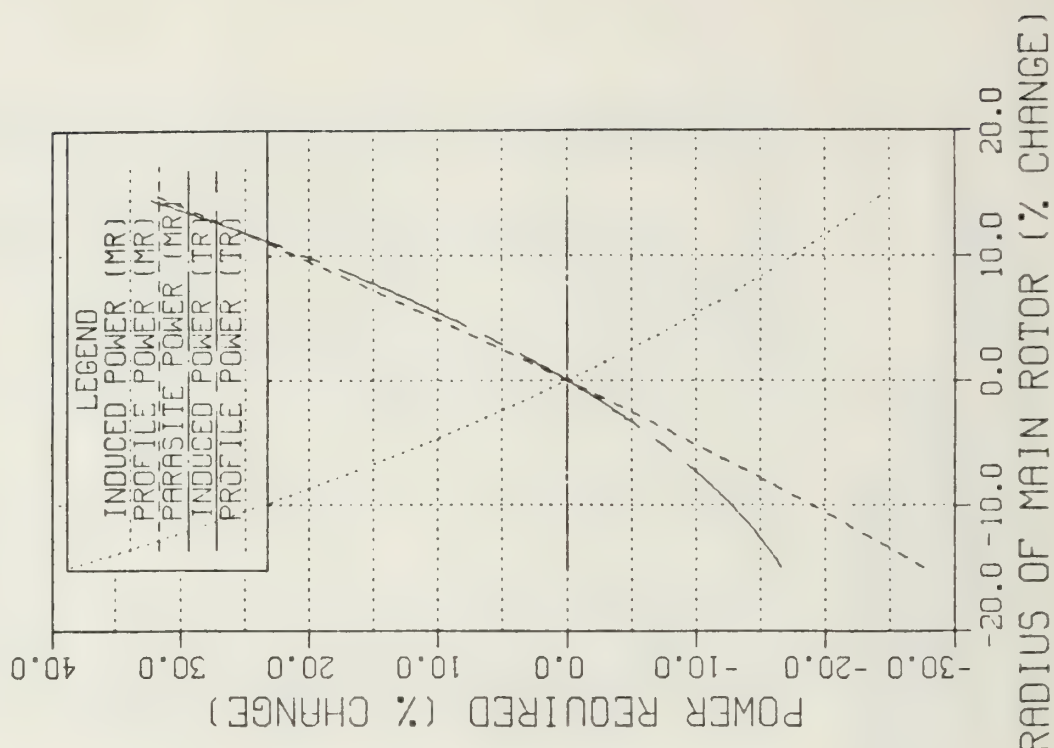
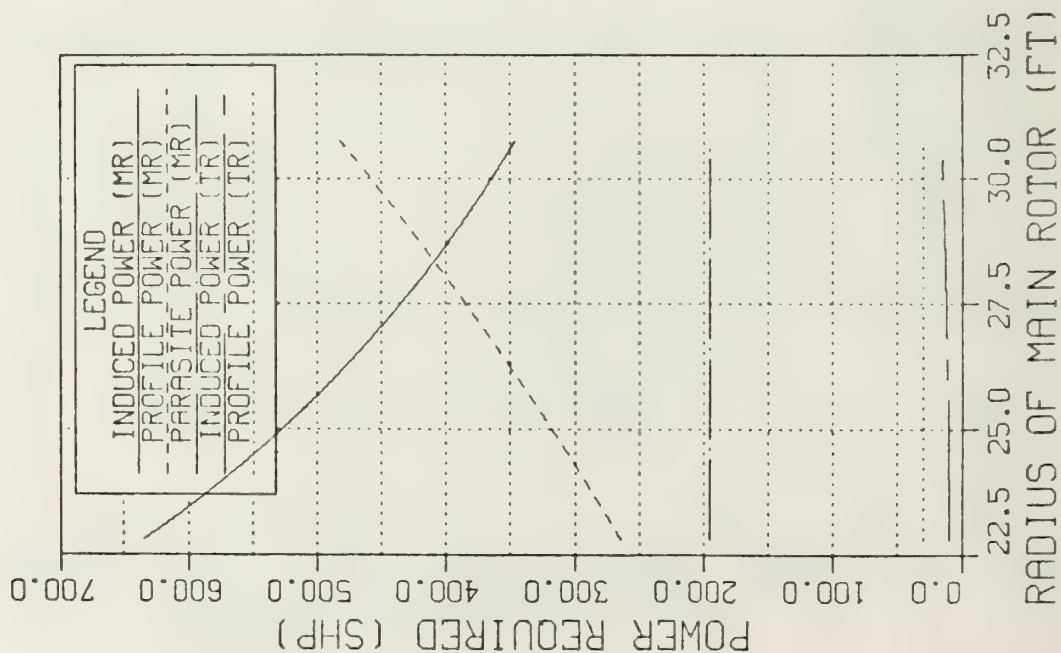
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CHORD, ADVANCE RATIO & TIP VELOCITY  
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# POWER VERSUS RADIUS

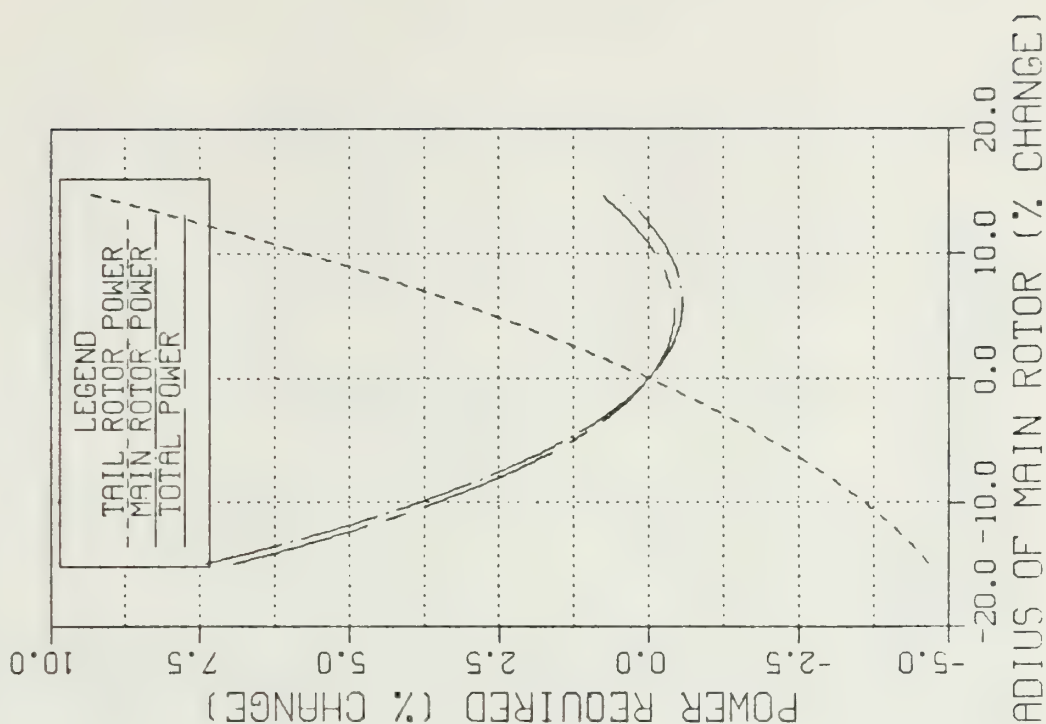
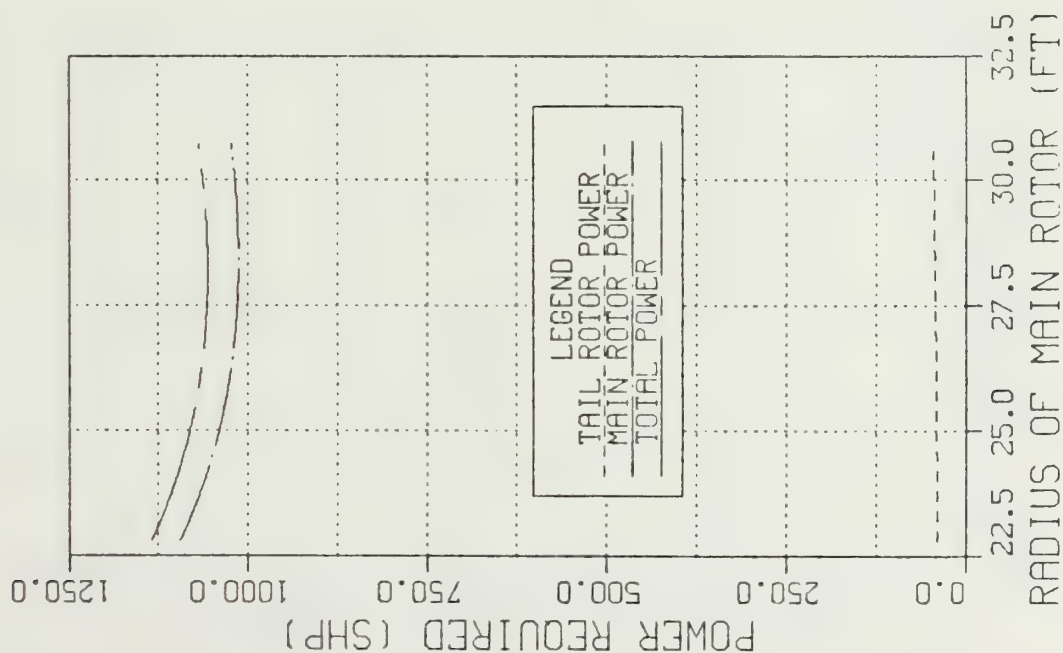
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# POWER VERSUS RADIUS

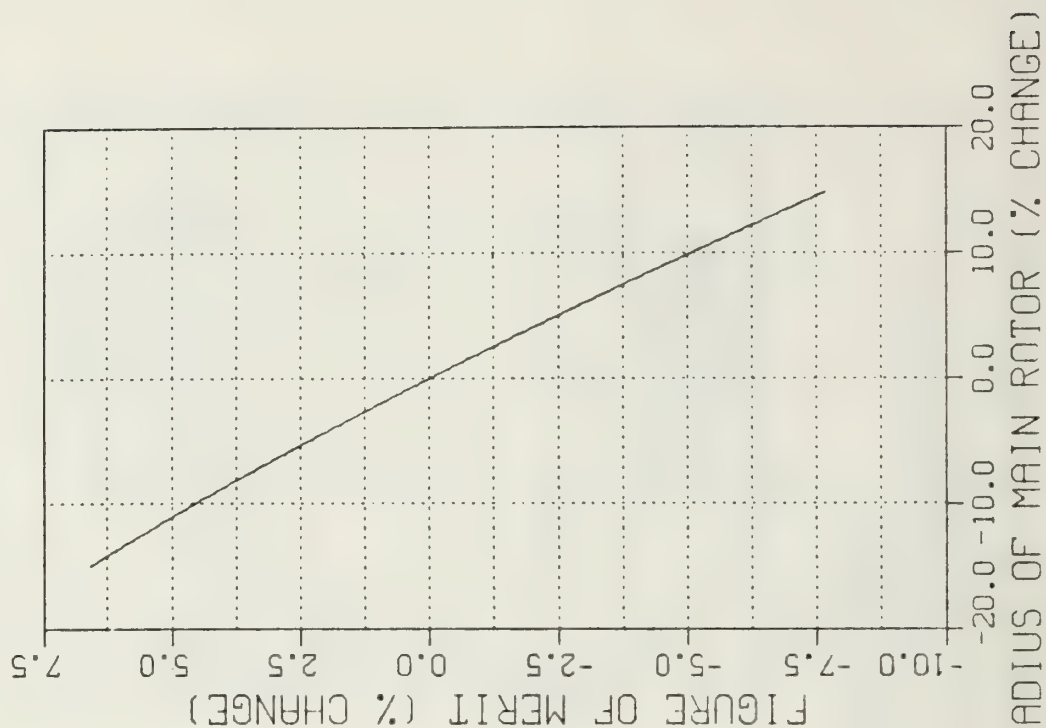
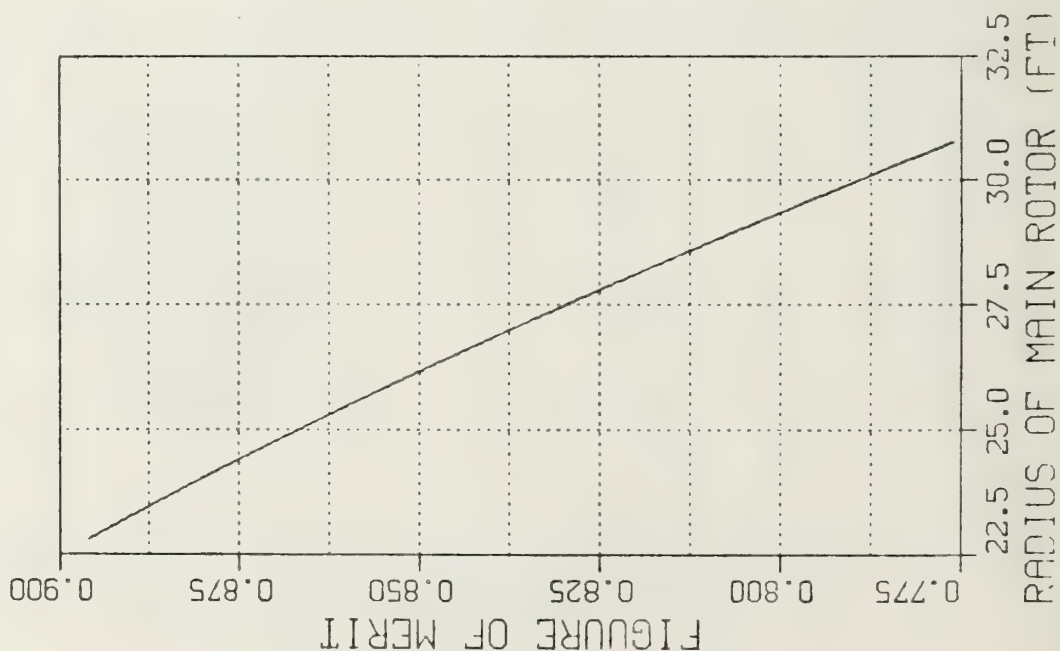
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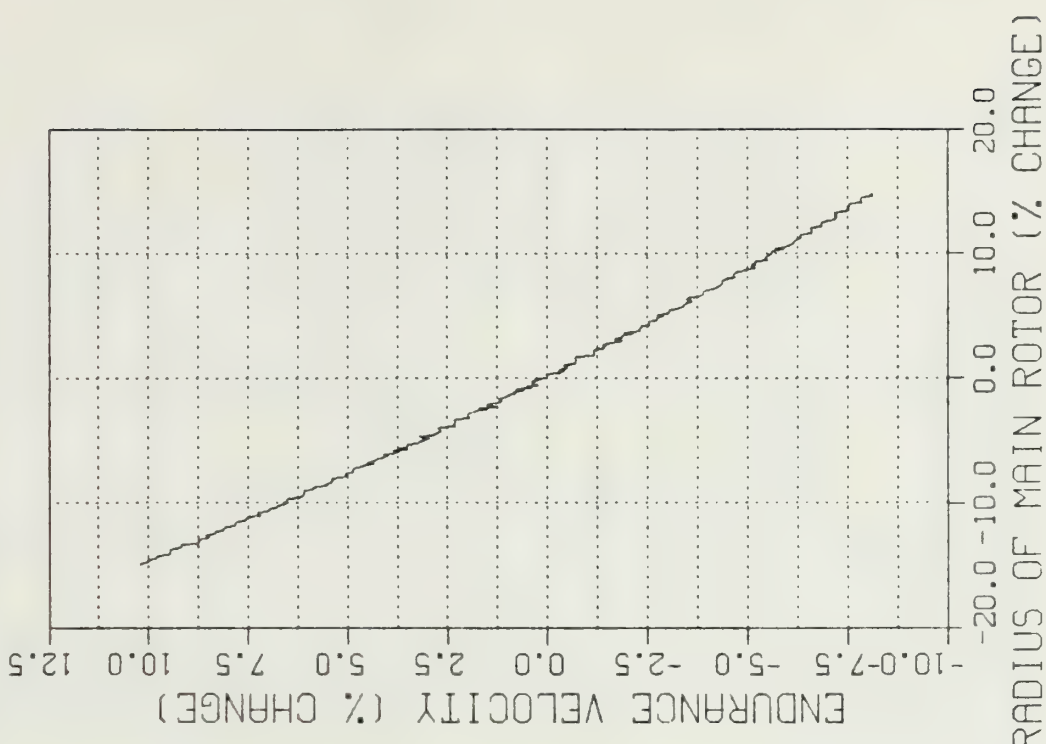
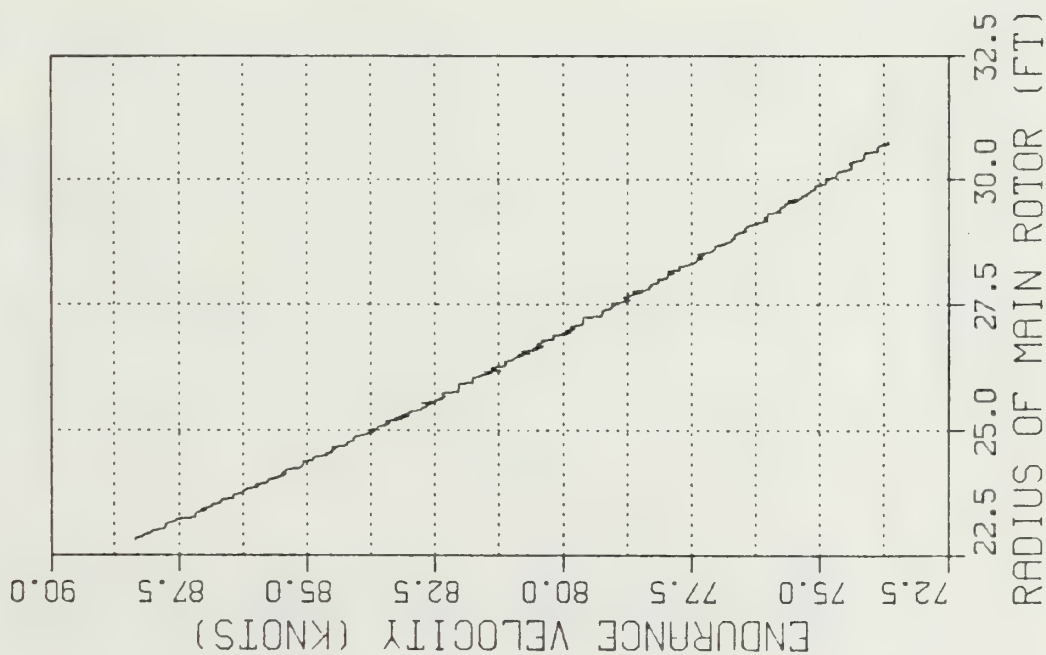
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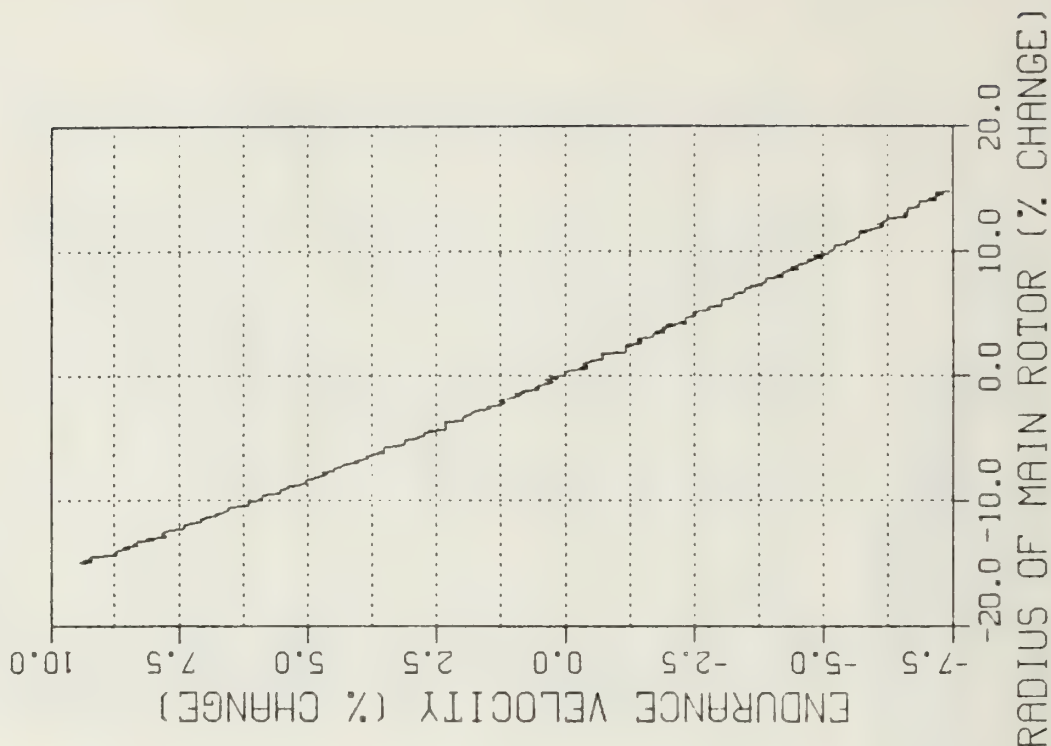
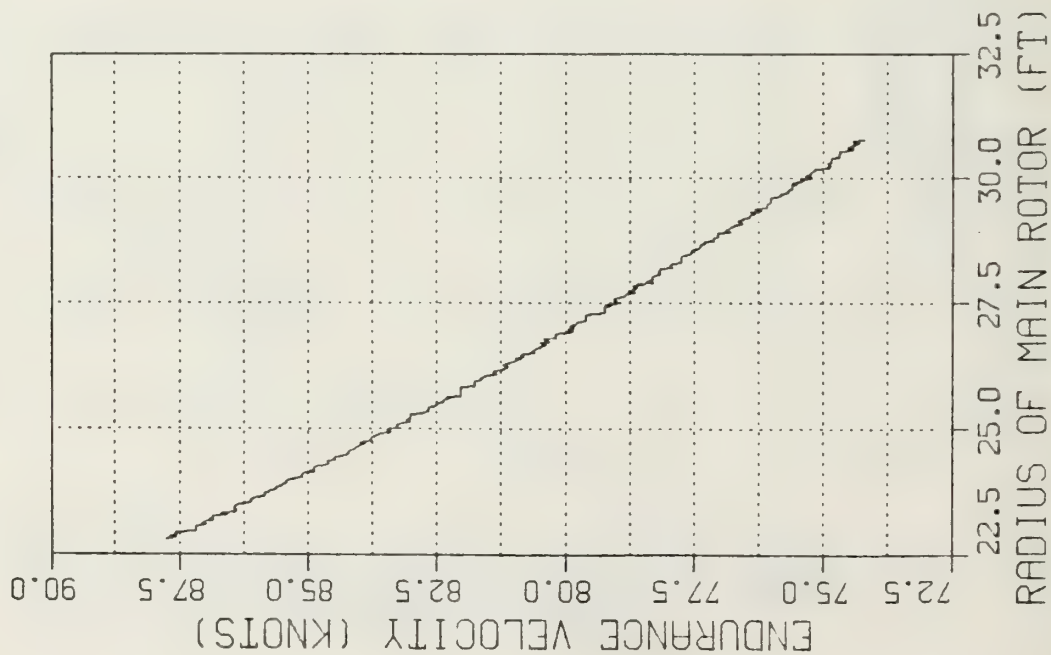
CHORD & ROTATIONAL VELOCITY  
ALLOWED TO VARY WITH RADIUS



# ENDURANCE VELOCITY VERSUS RADIUS CHORD & ROTATIONAL VELOCITY HELD CONSTANT SOLIDITY, TIP VELOCITY & ADVANCE RATIO ALLOWED TO VARY WITH RADIUS

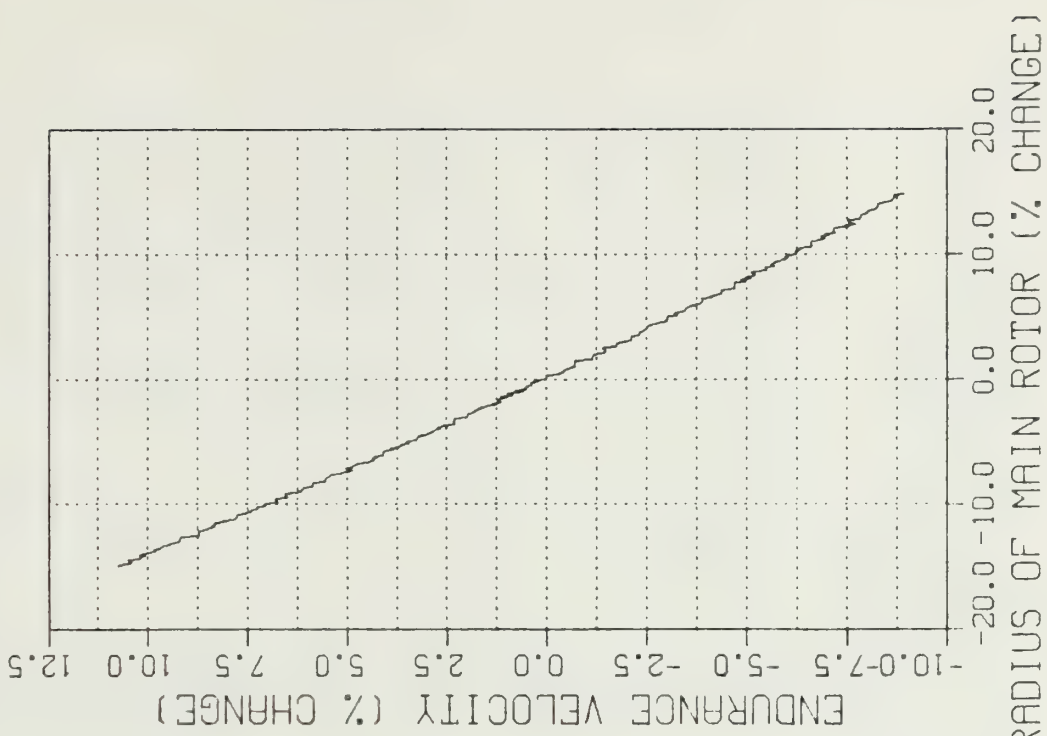
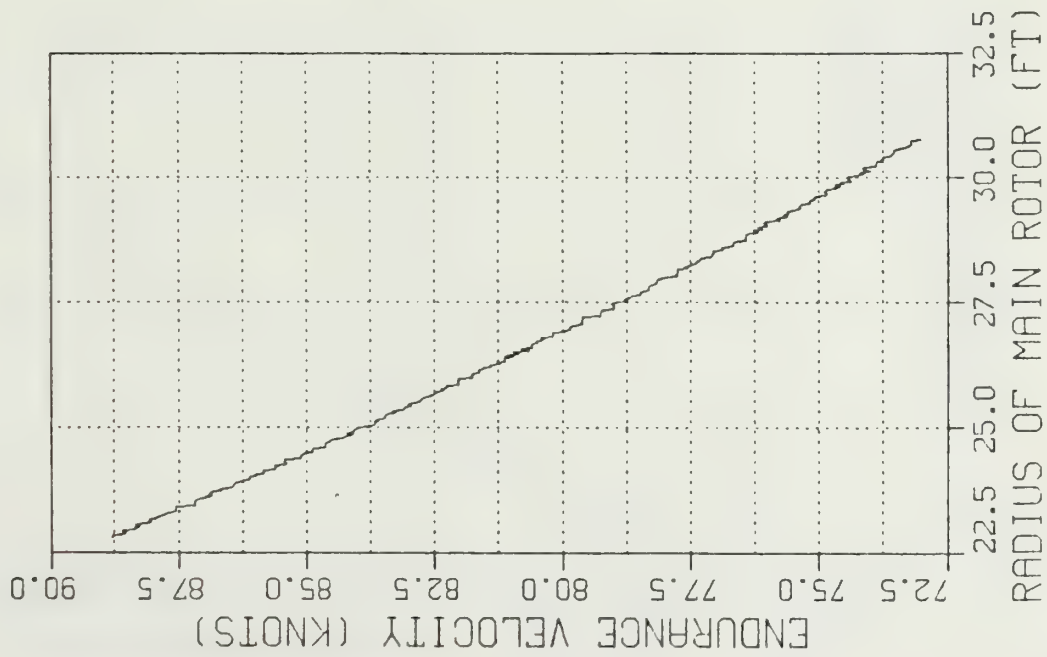


# ENDURANCE VELOCITY VERSUS RADIUS CHORD, TIP VELOCITY & ADVANCE RATIO HELD CONSTANT SOLIDITY, ROTATIONAL VELOCITY ALLOWED TO VARY WITH RADIUS

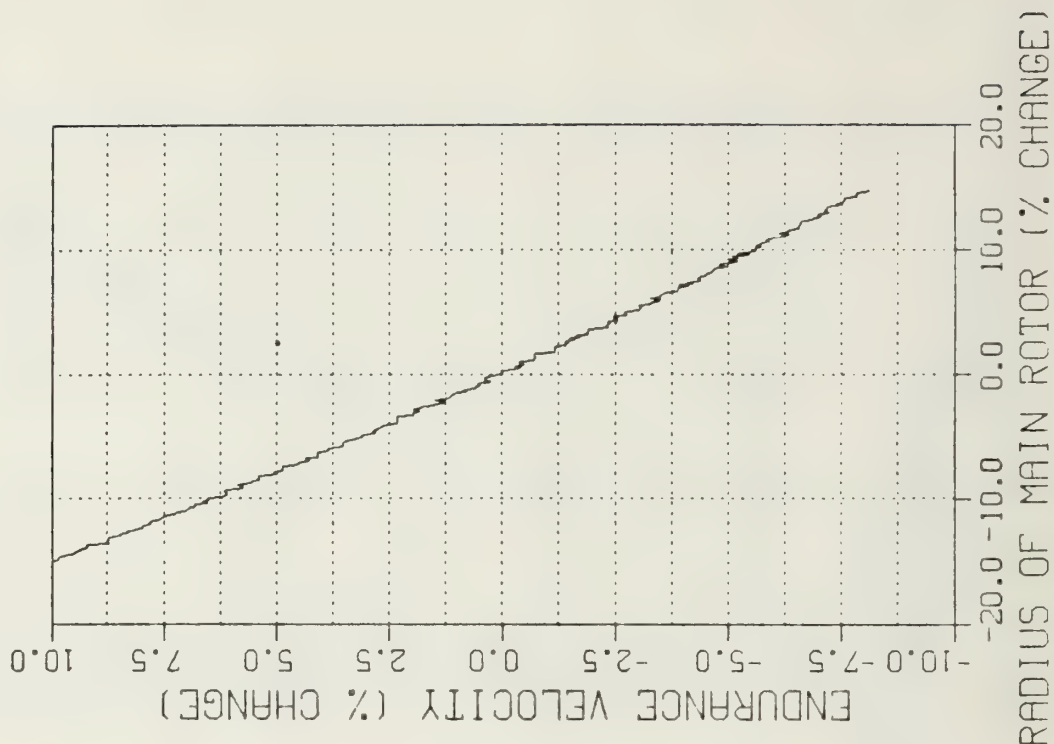
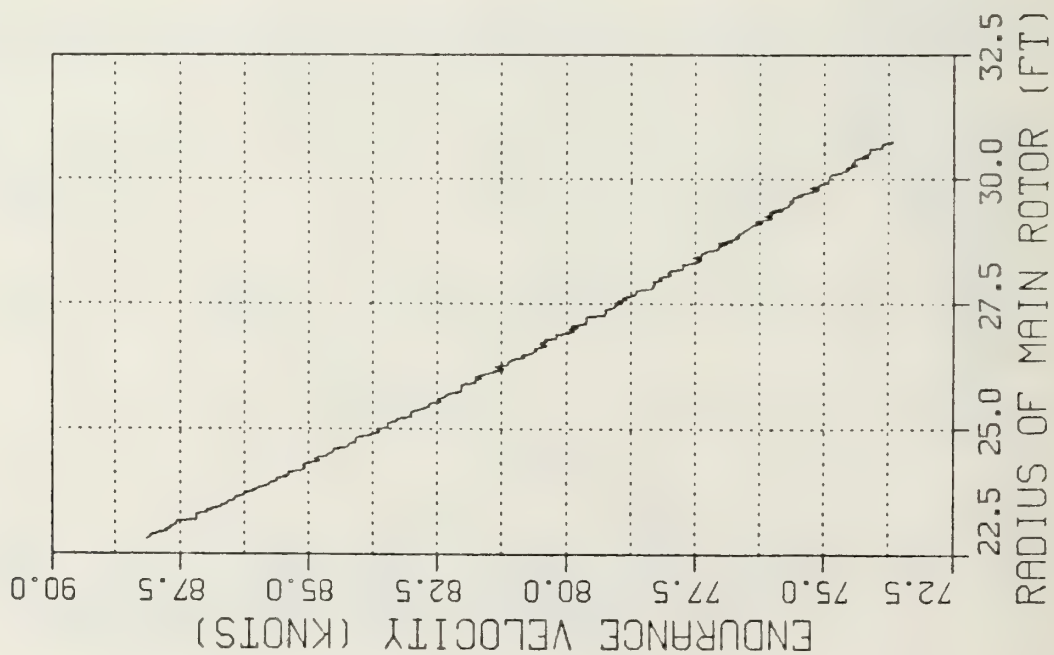




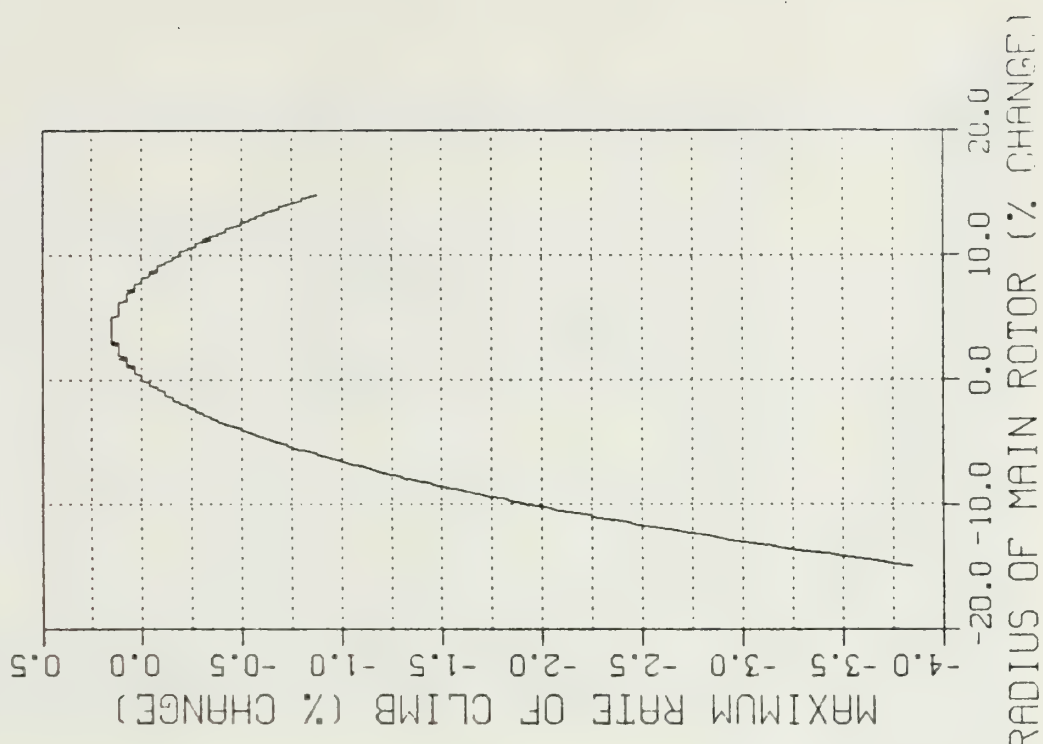
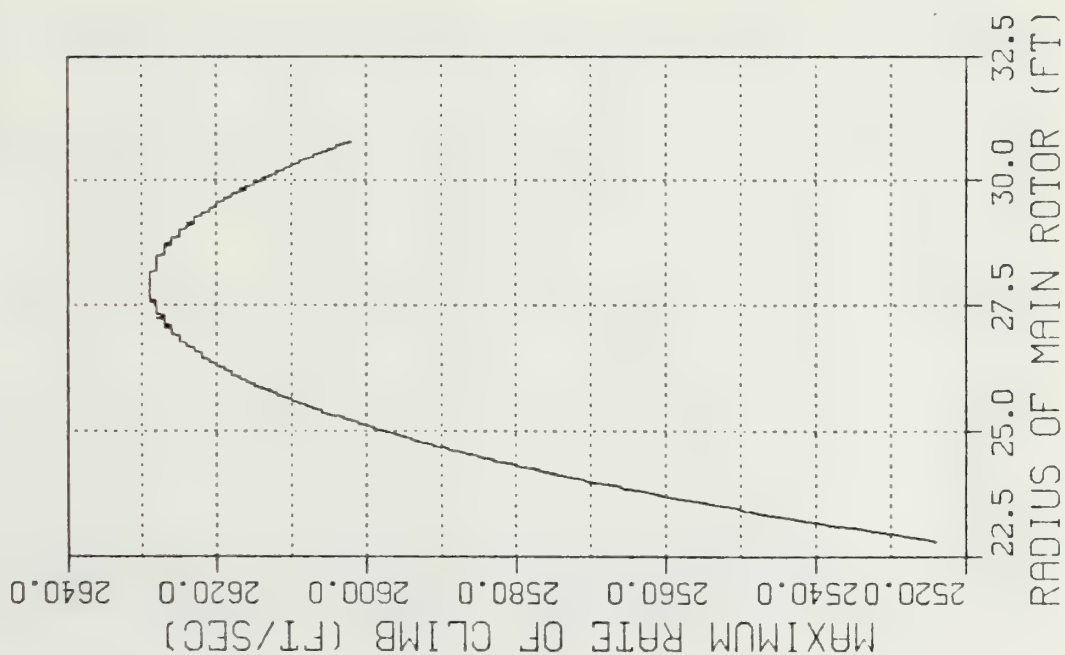
# ENDURANCE VELOCITY VERSUS RADIUS SOLIDITY & ROTATIONAL VELOCITY HELD CONSTANT CHORD, ADVANCE RATIO & TIP VELOCITY ALLOWED TO VARY WITH RADIUS



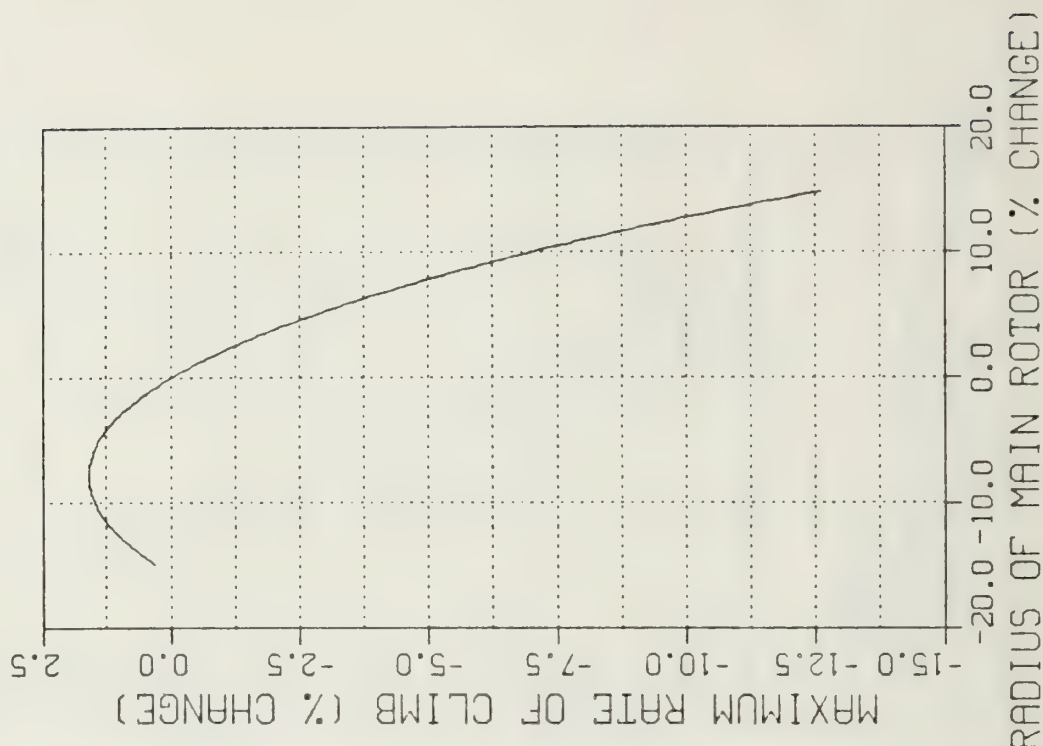
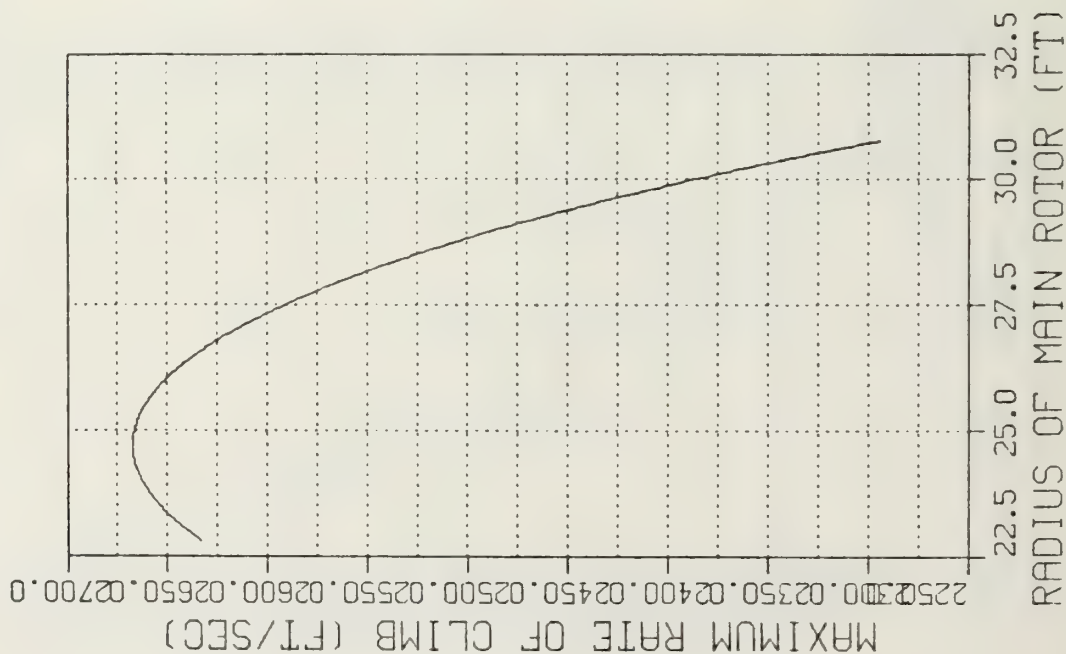
# ENDURANCE VELOCITY VERSUS RADIUS SOLIDITY, ADVANCE RATIO & TIP VELOCITY HELD CONSTANT CHORD & ROTATIONAL VELOCITY ALLOWED TO VARY WITH RADIUS



# MAXIMUM RATE OF CLIMB VERSUS RADIUS CHANGE SOLIDITY, ADVANCE RATIO & TIP VELOCITY HELD CONSTANT CHORD & ROTATIONAL VELOCITY ALLOWED TO VARY WITH RADIUS

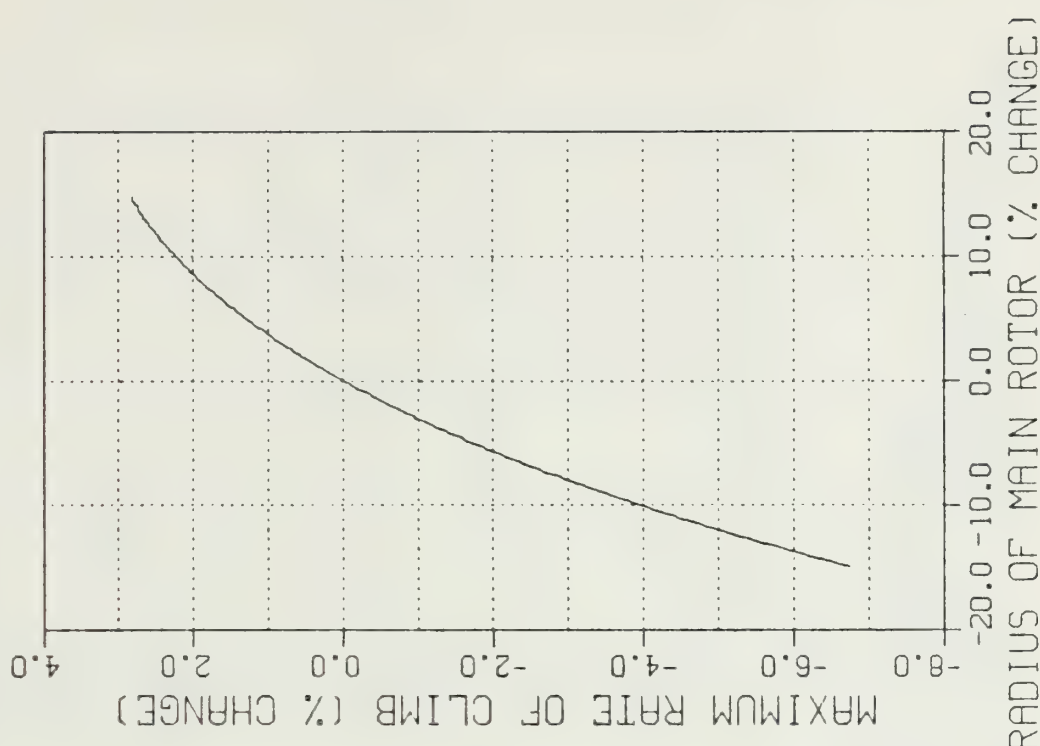
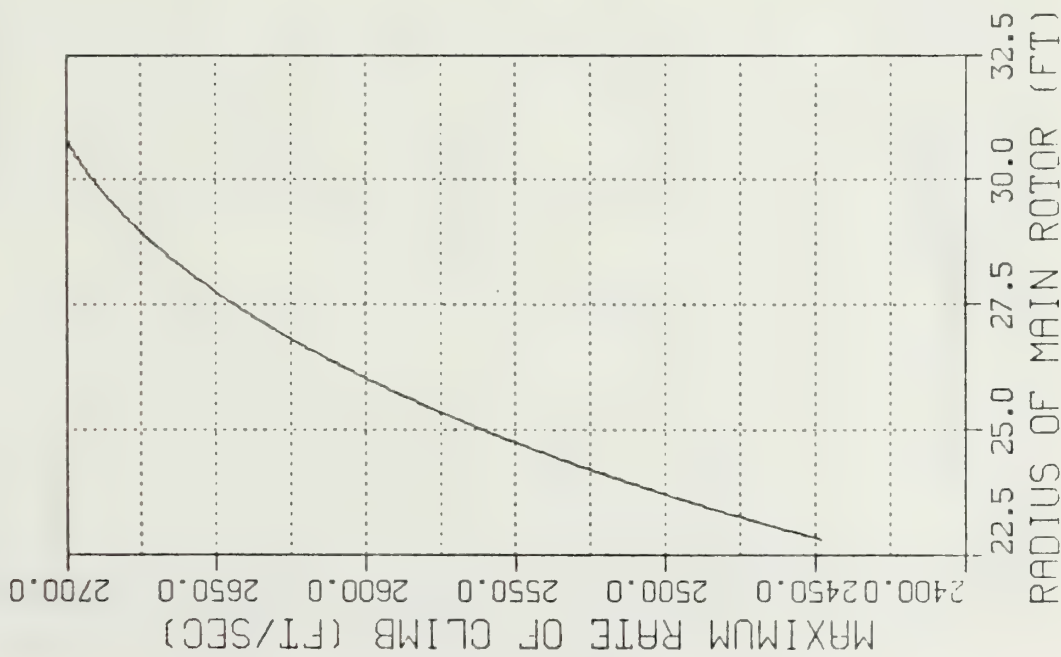


# MAXIMUM RATE OF CLIMB VERSUS RADIUS CHANGE SOLIDITY & ROTATIONAL VELOCITY HELD CONSTANT CHORD, ADVANCE RATIO & TIP VELOCITY ALLOWED TO VARY WITH RADIUS

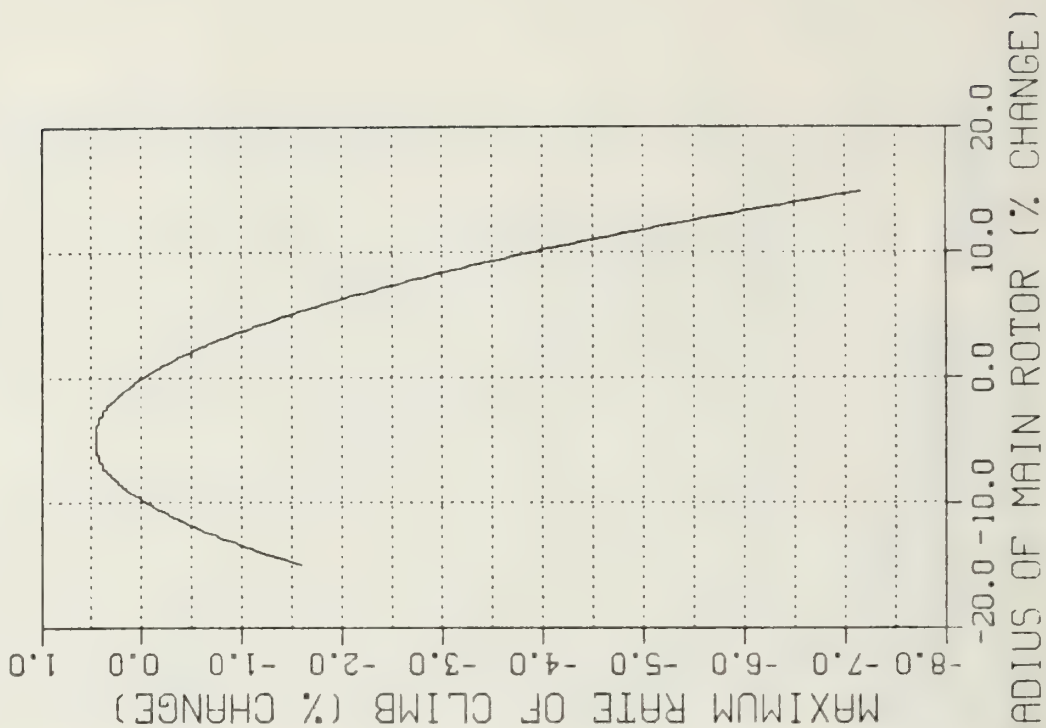
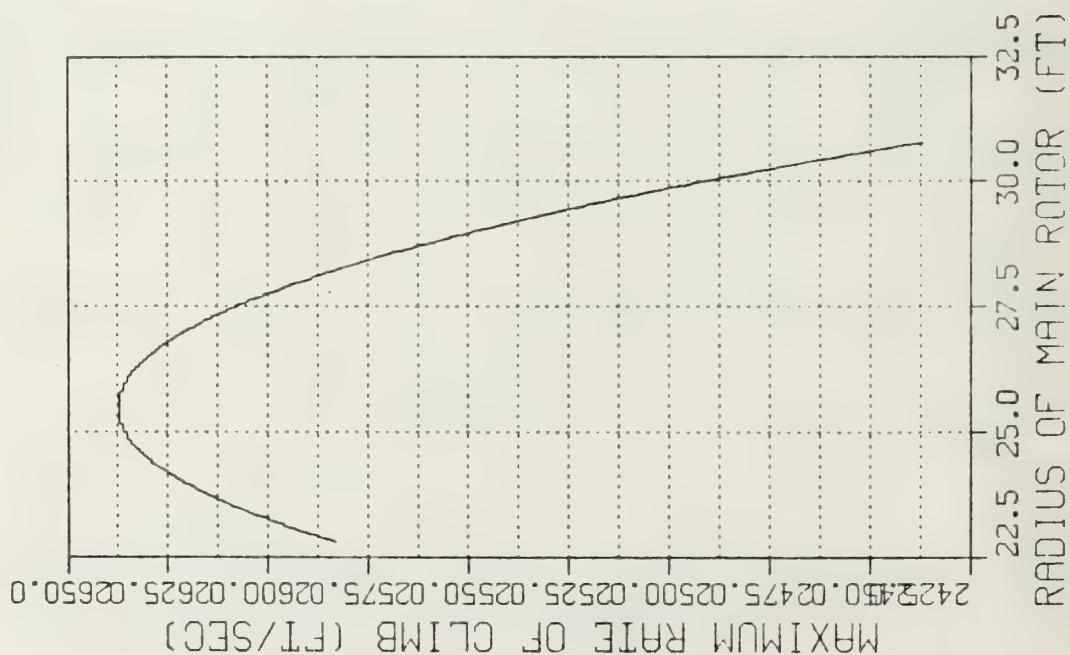




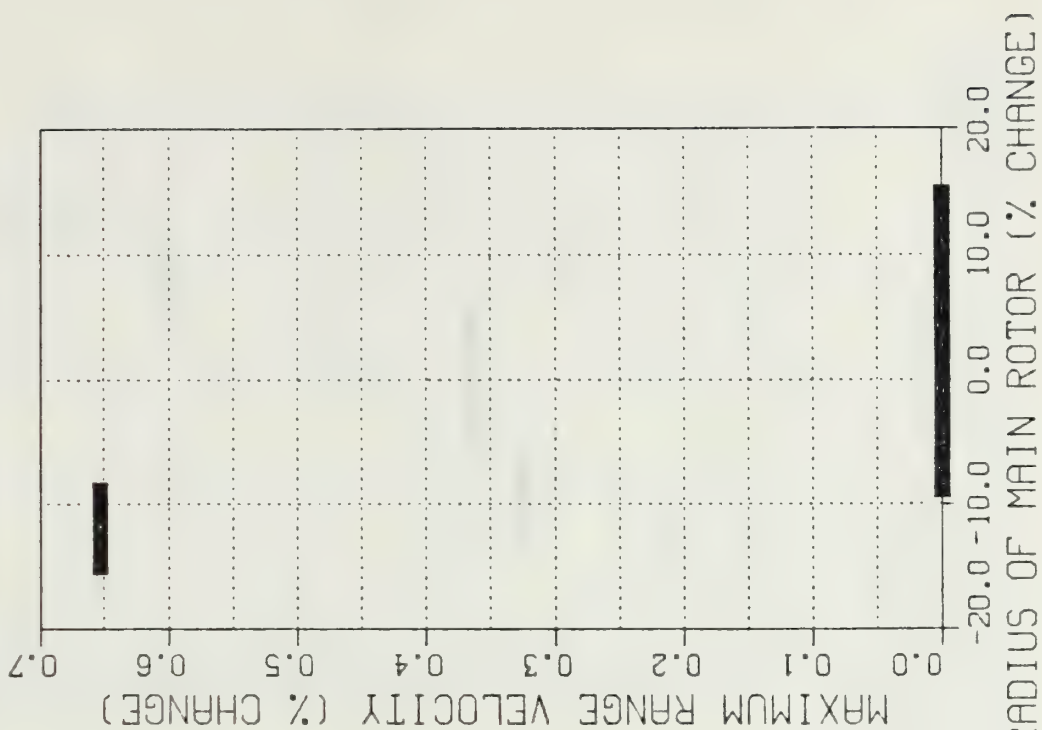
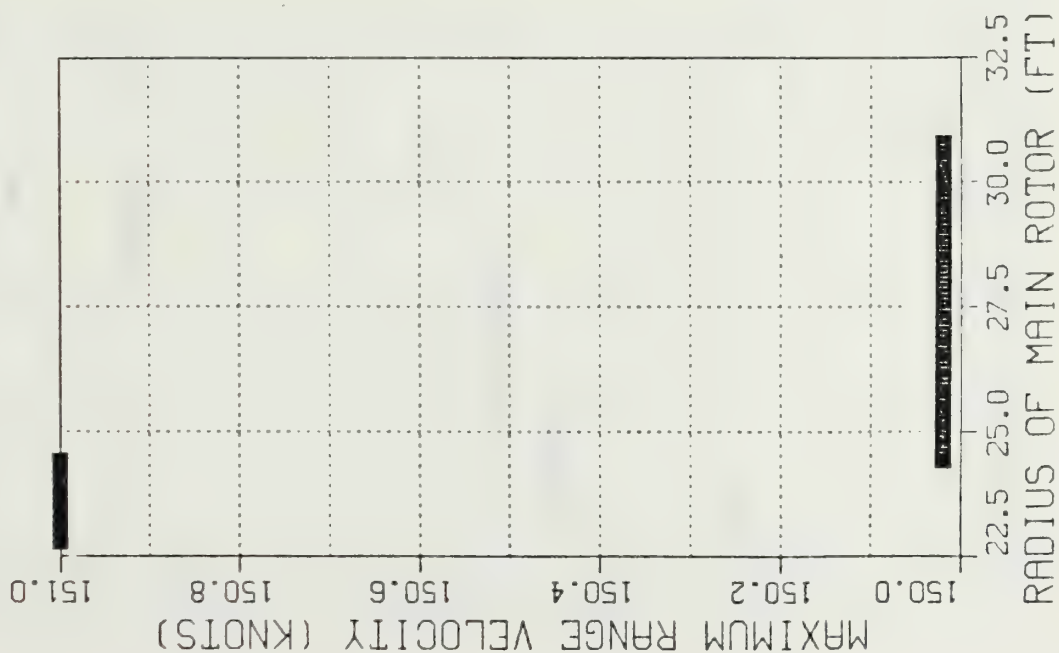
MAXIMUM RATE OF CLIMB VERSUS RADIUS CHANGE  
 CHORD, TIP VELOCITY & ADVANCE RATIO HELD CONSTANT  
 SOLIDITY, ROTATIONAL VELOCITY  
 ALLOWED TO VARY WITH RADIUS



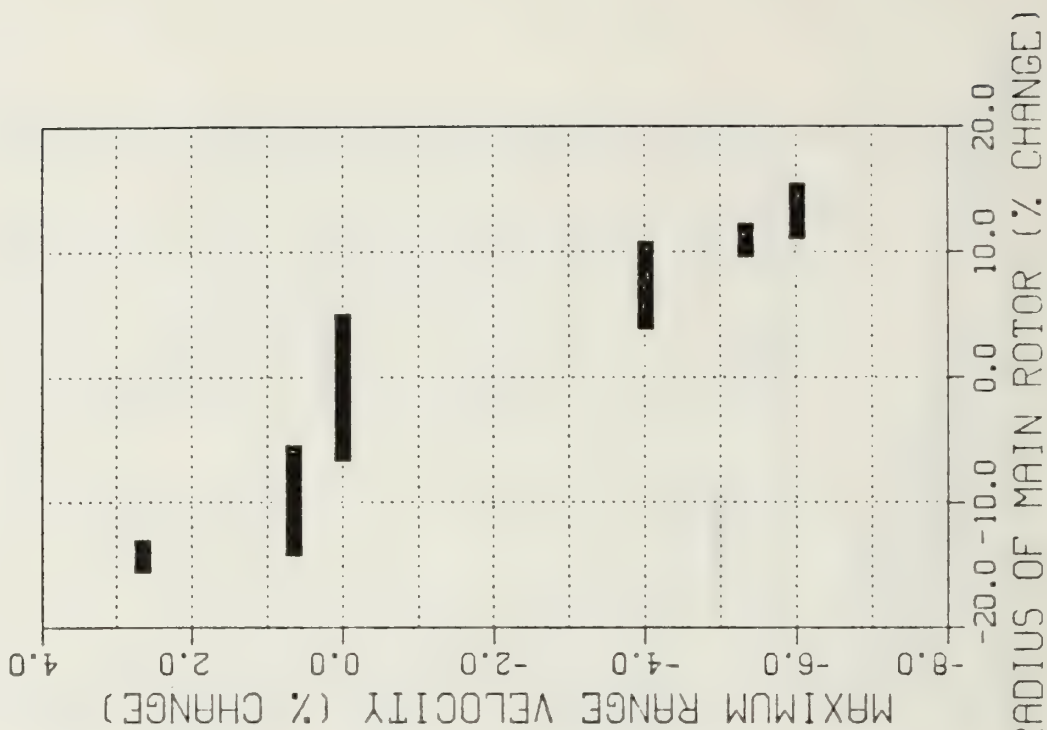
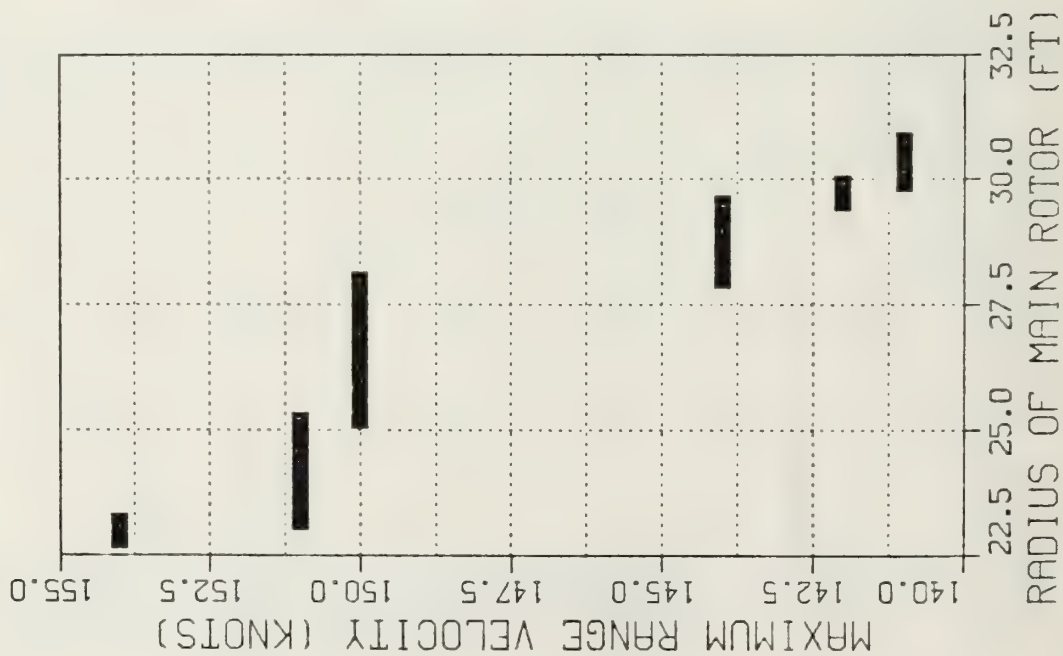
# MAXIMUM RATE OF CLIMB VERSUS RADIUS CHANGE CHORD & ROTATIONAL VELOCITY HELD CONSTANT SOLIDITY, TIP VELOCITY & ADVANCE RATIO ALLOWED TO VARY WITH RADIUS



# MAXIMUM RANGE VELOCITY VERSUS RADIUS CHANGE CHORD & ROTATIONAL VELOCITY HELD CONSTANT SOLIDITY, TIP VELOCITY & ADVANCE RATIO ALLOWED TO VARY WITH RADIUS

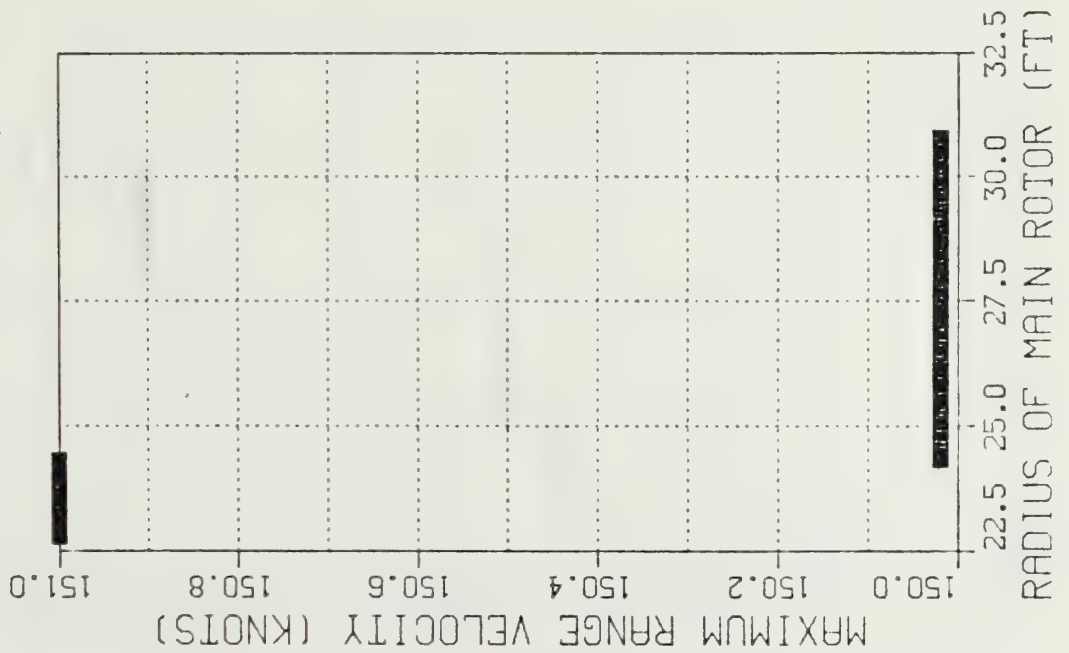


# MAXIMUM RANGE VELOCITY VERSUS RADIUS CHANGE CHORD, TIP VELOCITY & ADVANCE RATIO HELD CONSTANT SOLIDITY, ROTATIONAL VELOCITY ALLOWED TO VARY WITH RADIUS

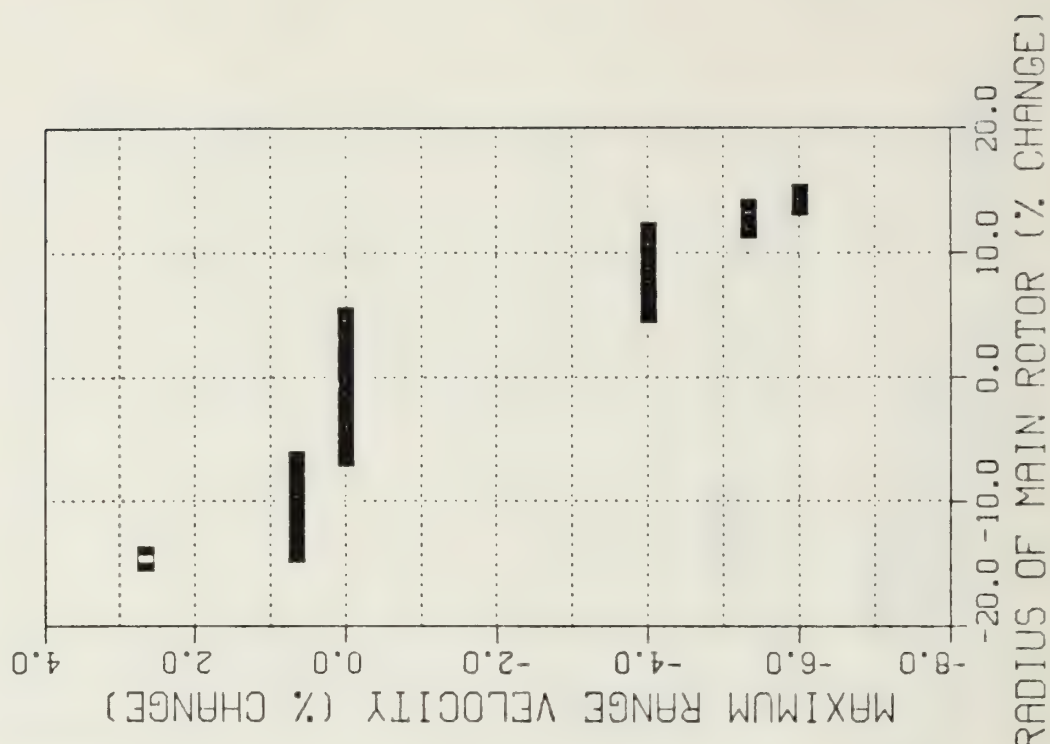
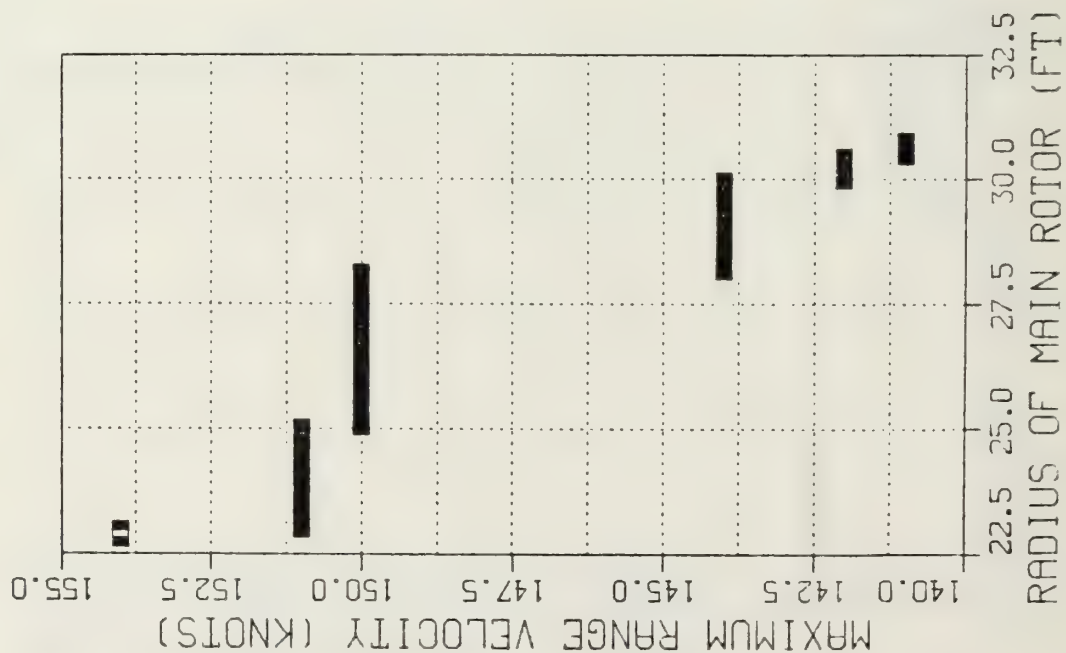




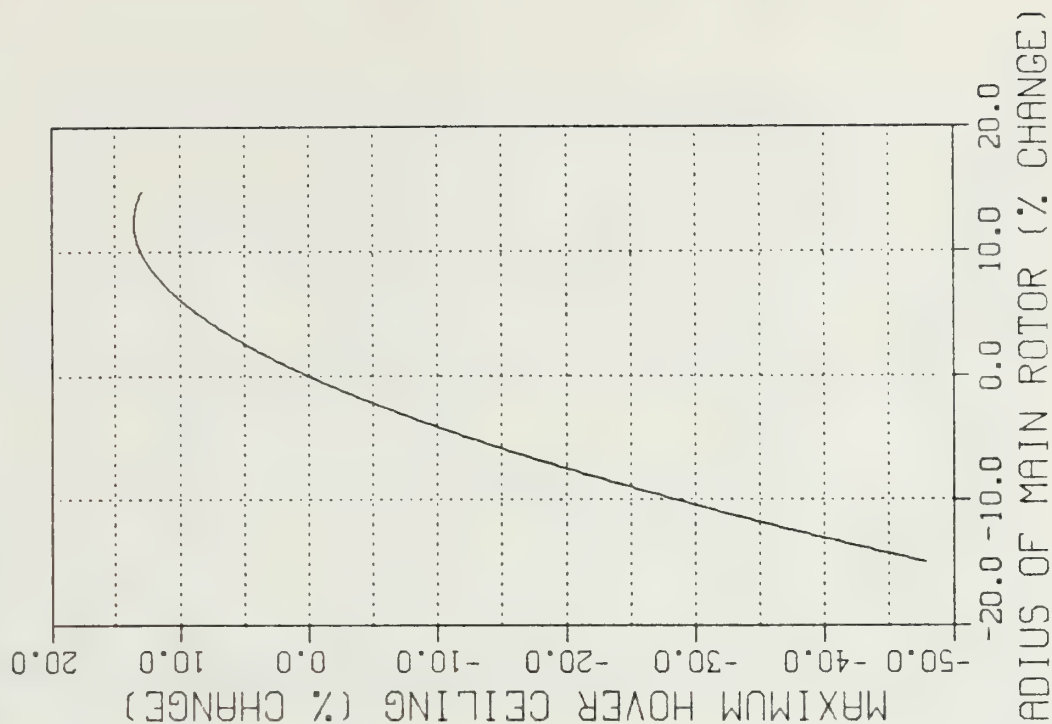
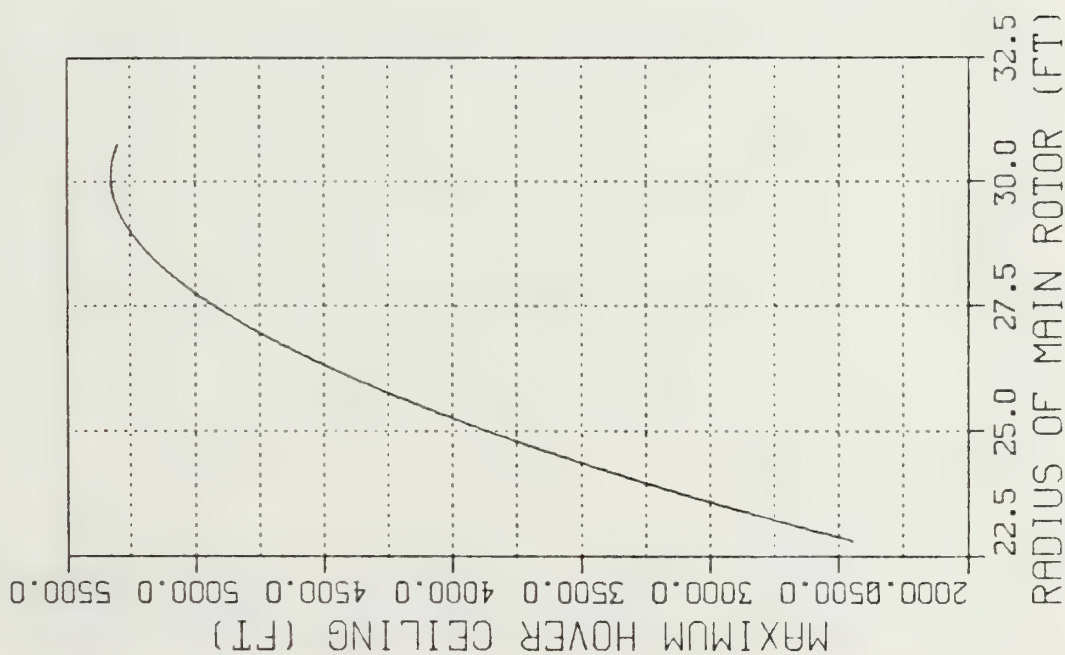
# MAXIMUM RANGE VELOCITY VERSUS RADIUS CHANGE SOLIDITY & ROTATIONAL VELOCITY HELD CONSTANT CHORD, ADVANCE RATIO & TIP VELOCITY ALLOWED TO VARY WITH RADIUS



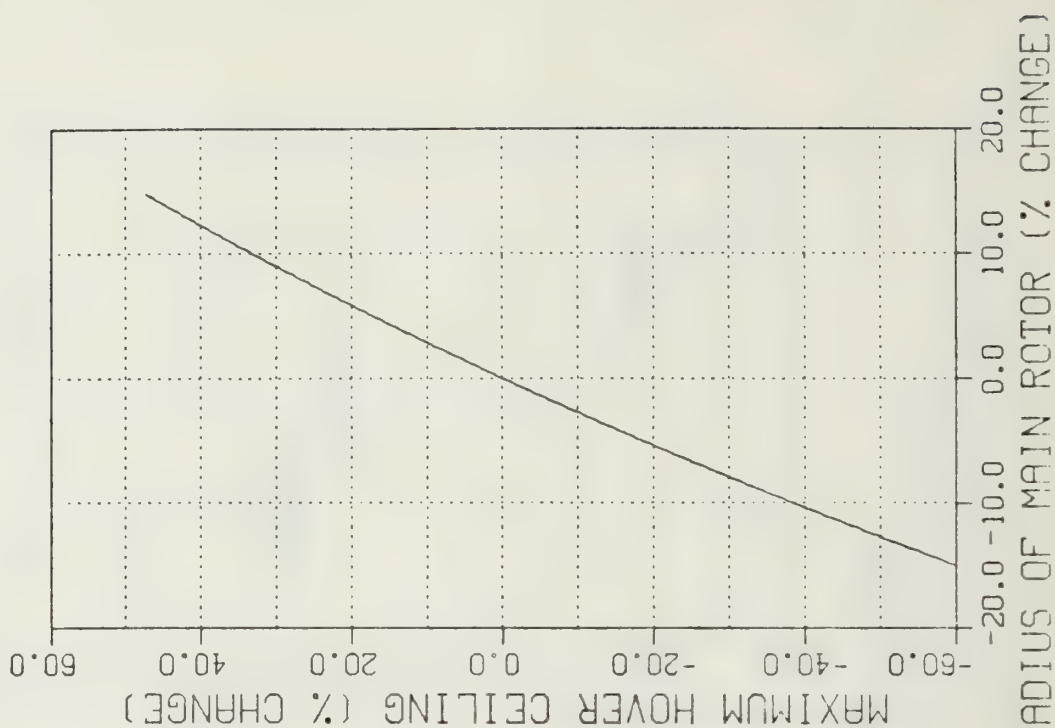
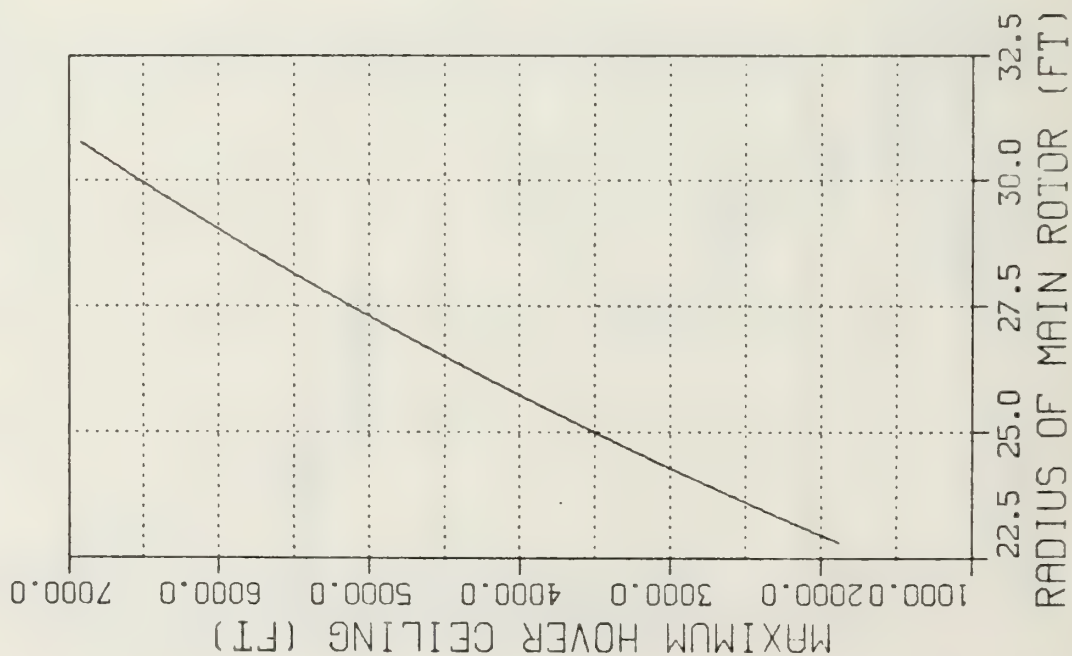
# MAXIMUM RANGE VELOCITY VERSUS RADIUS CHANGE SOLIDITY, ADVANCE RATIO & TIP VELOCITY HELD CONSTANT CHORD & ROTATIONAL VELOCITY ALLOWED TO VARY WITH RADIUS



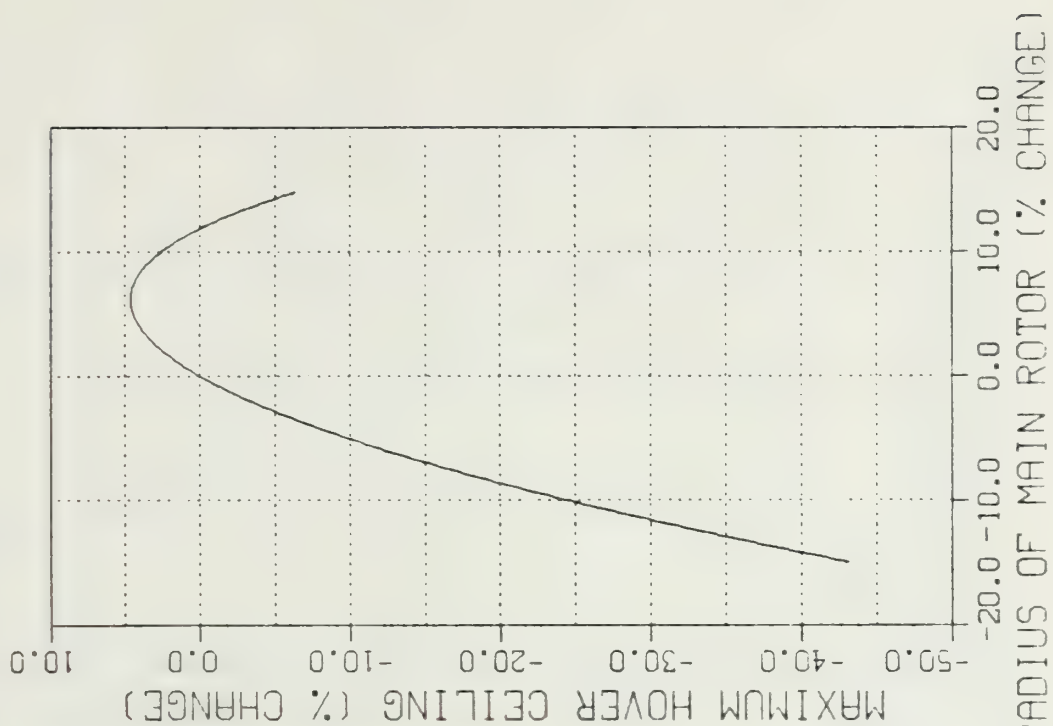
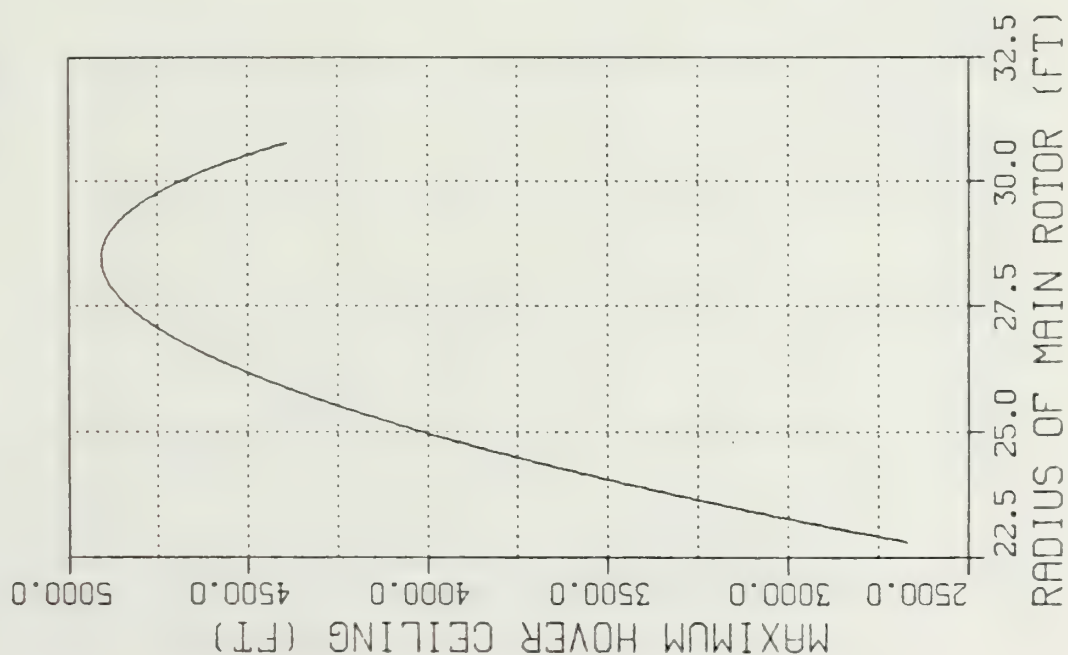
# MAXIMUM HOVER CEILING (IGE) VERSUS RADIUS CHORD & ROTATIONAL VELOCITY HELD CONSTANT SOLIDITY, TIP VELOCITY & ADVANCE RATIO ALLOWED TO VARY WITH RADIUS



MAXIMUM HOVER CEILING (IGE) VERSUS RADIUS  
 CHORD, TIP VELOCITY & ADVANCE RATIO HELD CONSTANT  
 SOLIDITY, ROTATIONAL VELOCITY  
 ALLOWED TO VARY WITH RADIUS

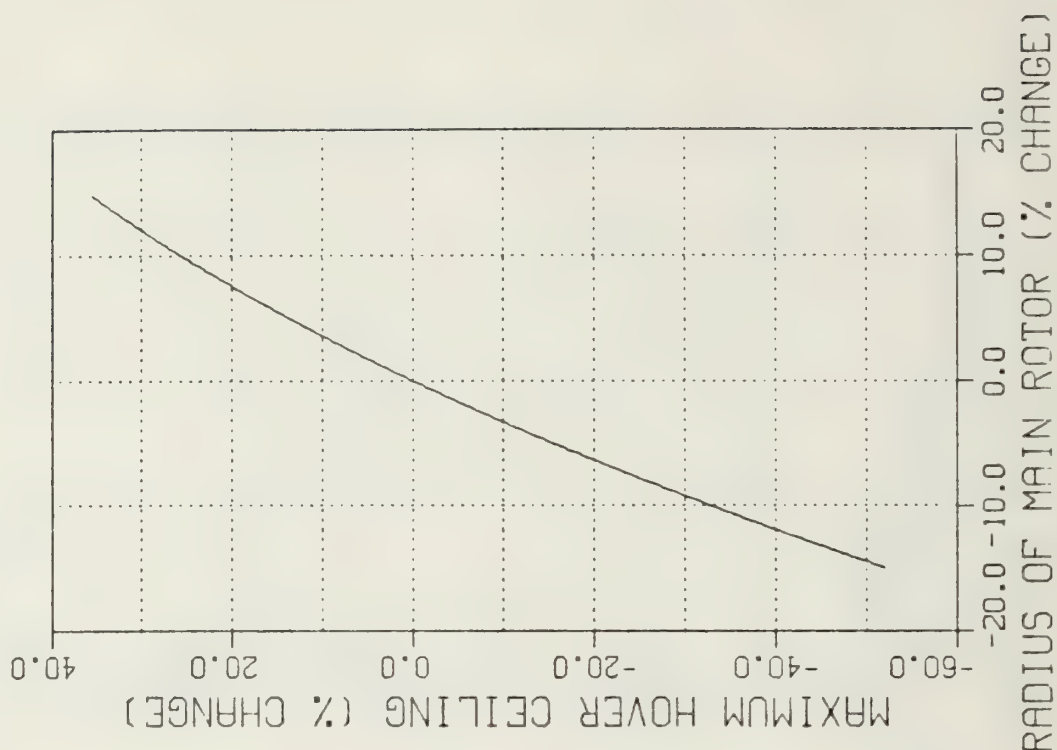
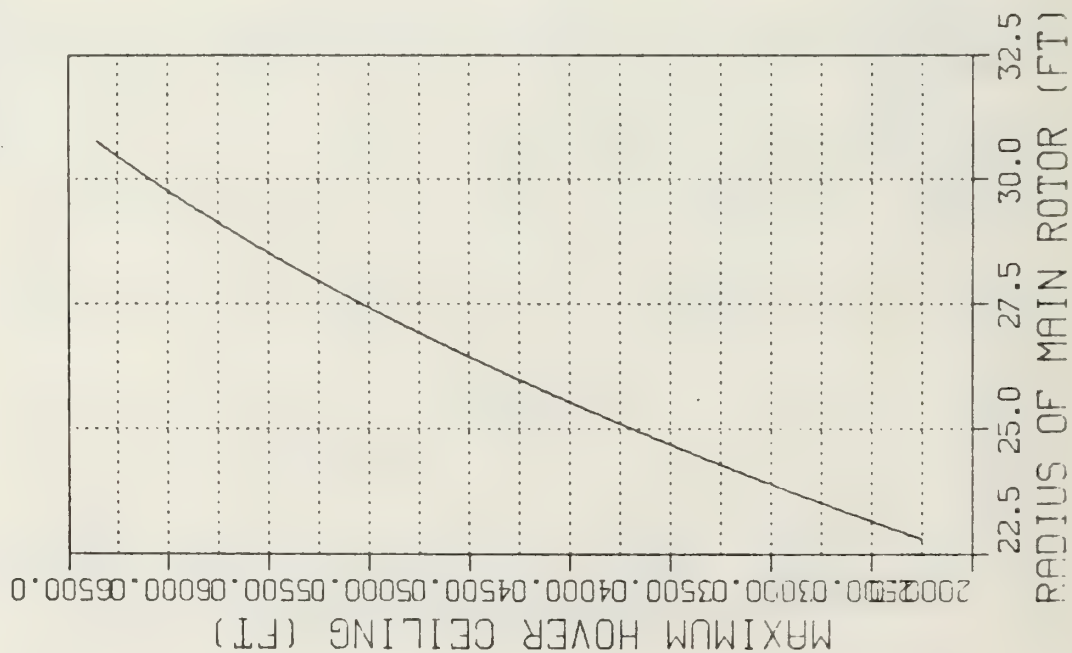


MAXIMUM HOVER CEILING (IGE) VERSUS RADIUS  
 SOLIDITY & ROTATIONAL VELOCITY HELD CONSTANT  
 CHORD, ADVANCE RATIO & TIP VELOCITY  
 ALLOWED TO VARY WITH RADIUS

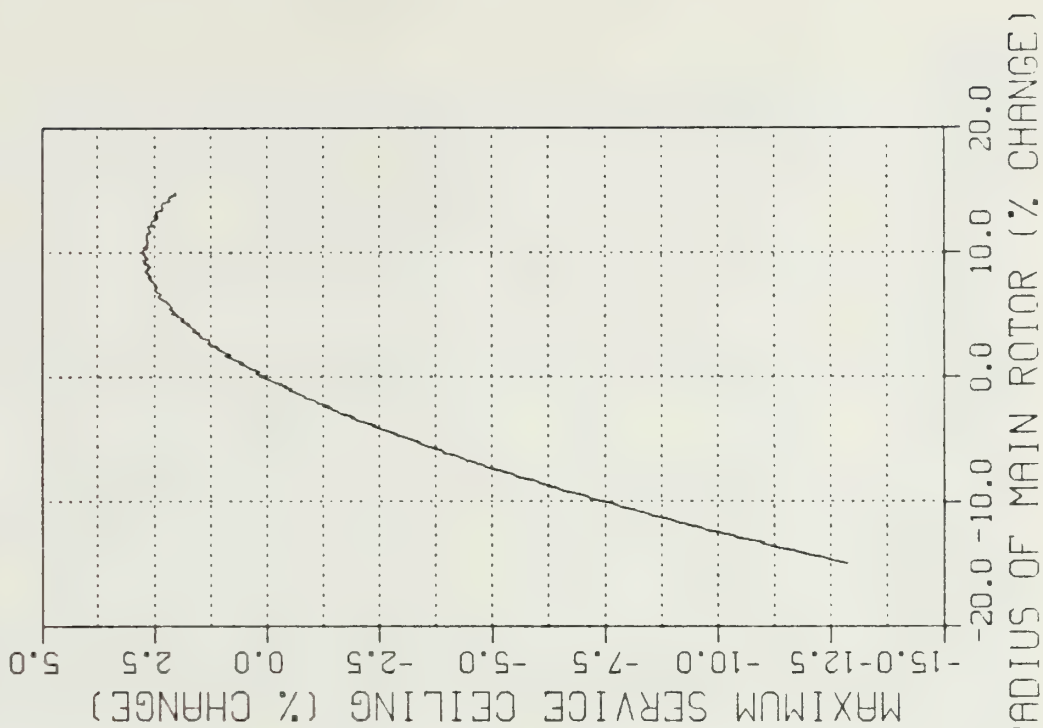
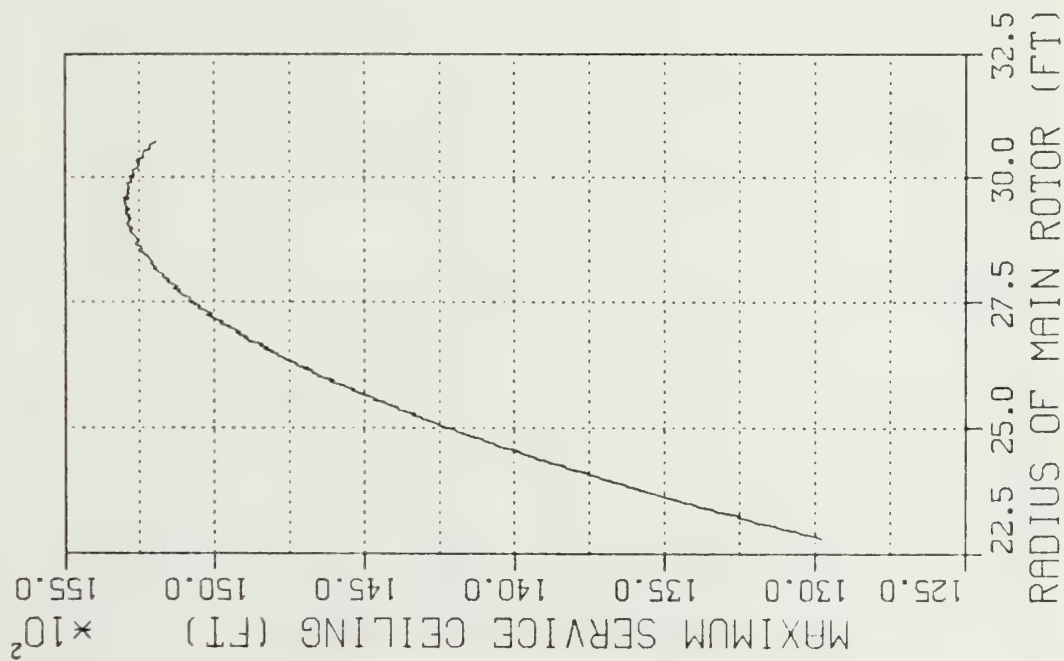




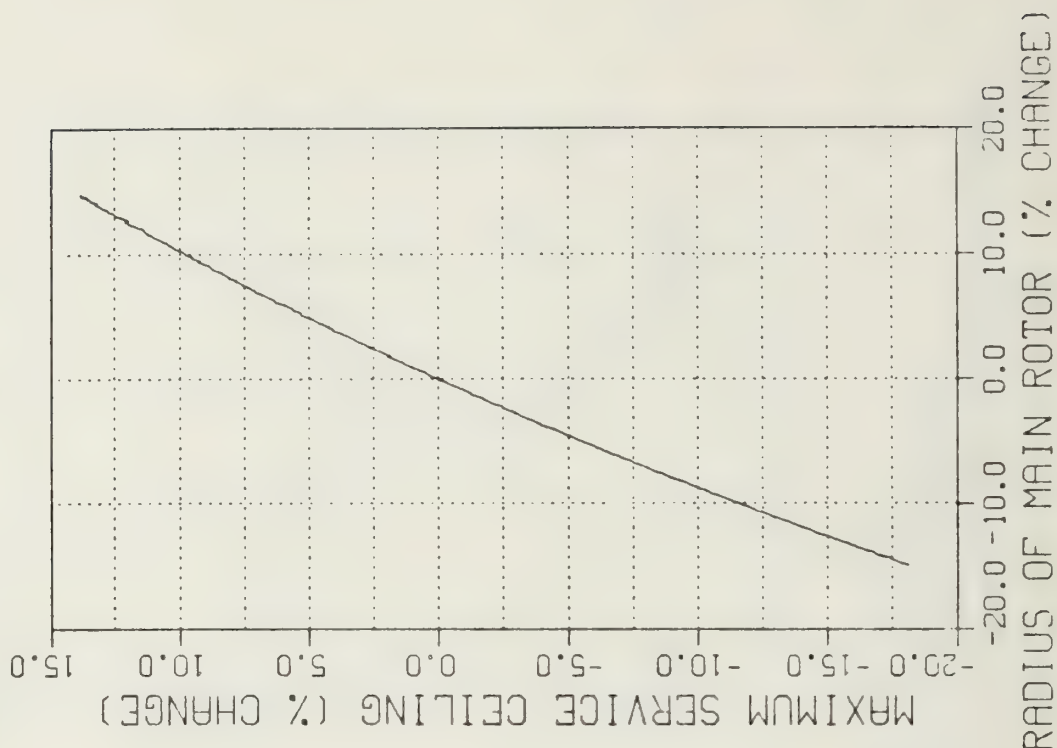
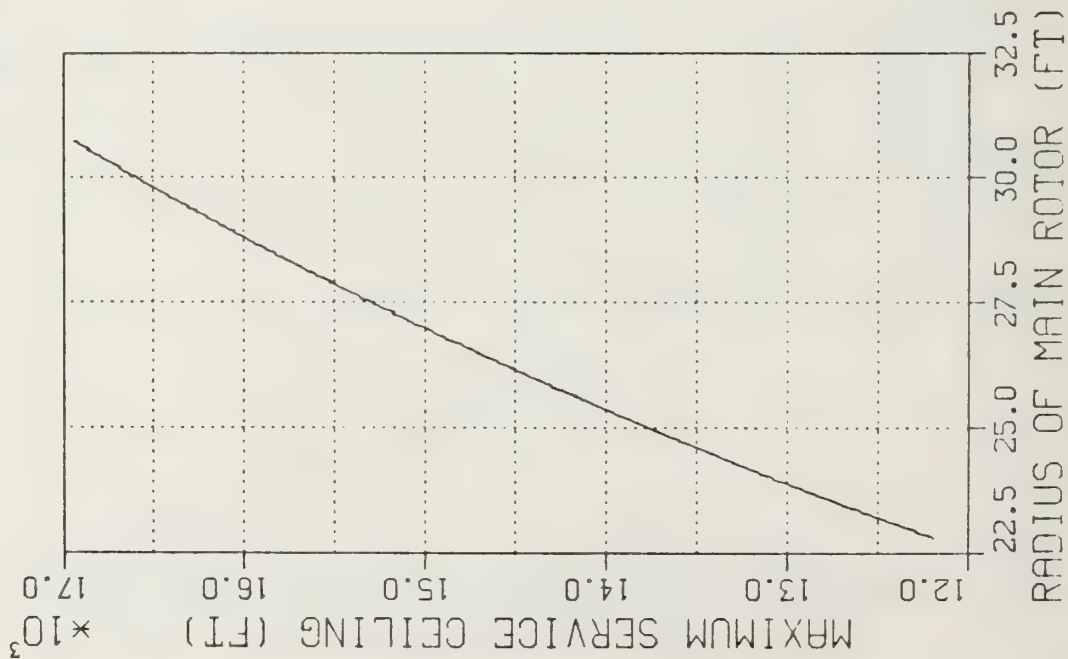
# MAXIMUM HOVER CEILING (IGE) VERSUS RADIUS SOLIDITY, ADVANCE RATIO & TIP VELOCITY HELD CONSTANT CHORD & ROTATIONAL VELOCITY ALLOWED TO VARY WITH RADIUS



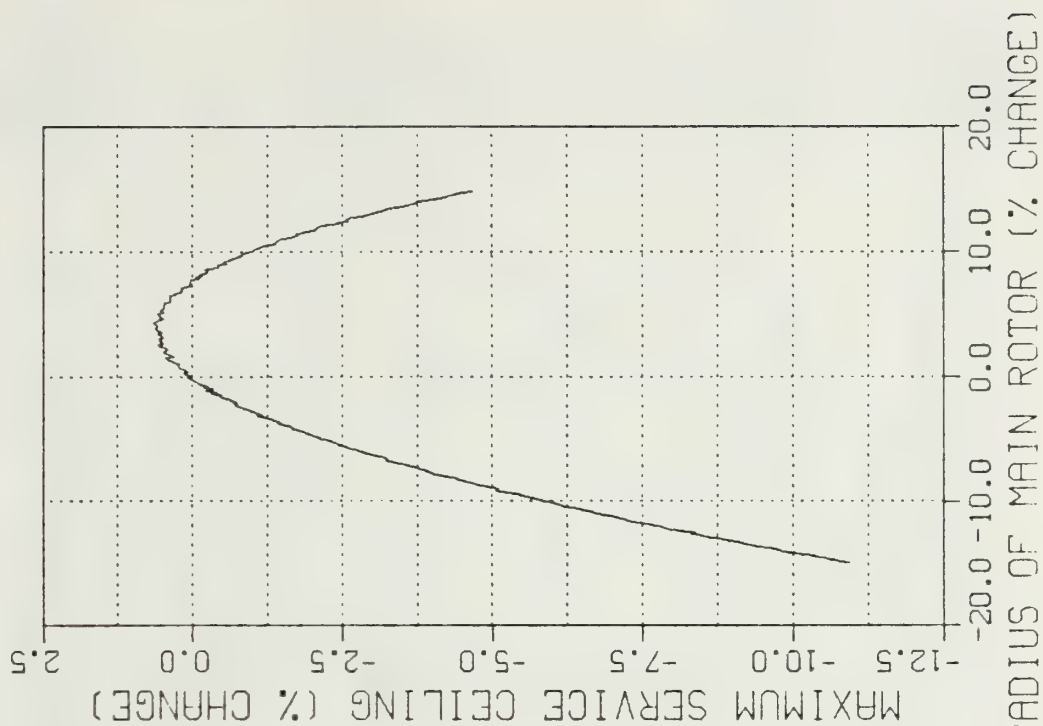
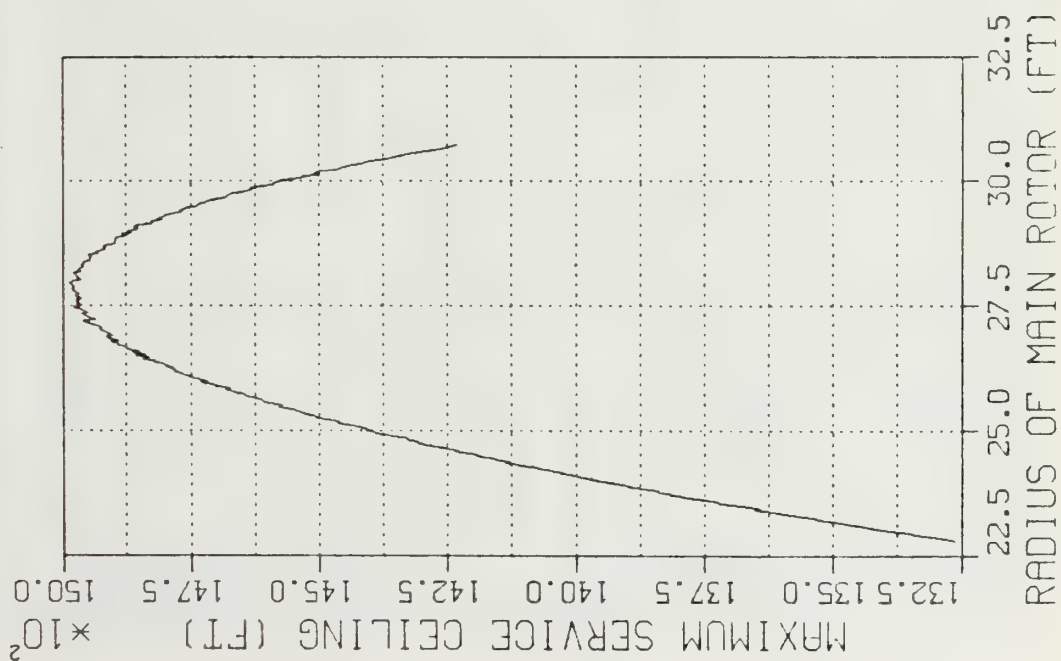
# MAXIMUM SERVICE CEILING VERSUS RADIUS CHANGE CHORD & ROTATIONAL VELOCITY HELD CONSTANT SOLIDITY, TIP VELOCITY & ADVANCE RATIO ALLOWED TO VARY WITH RADIUS



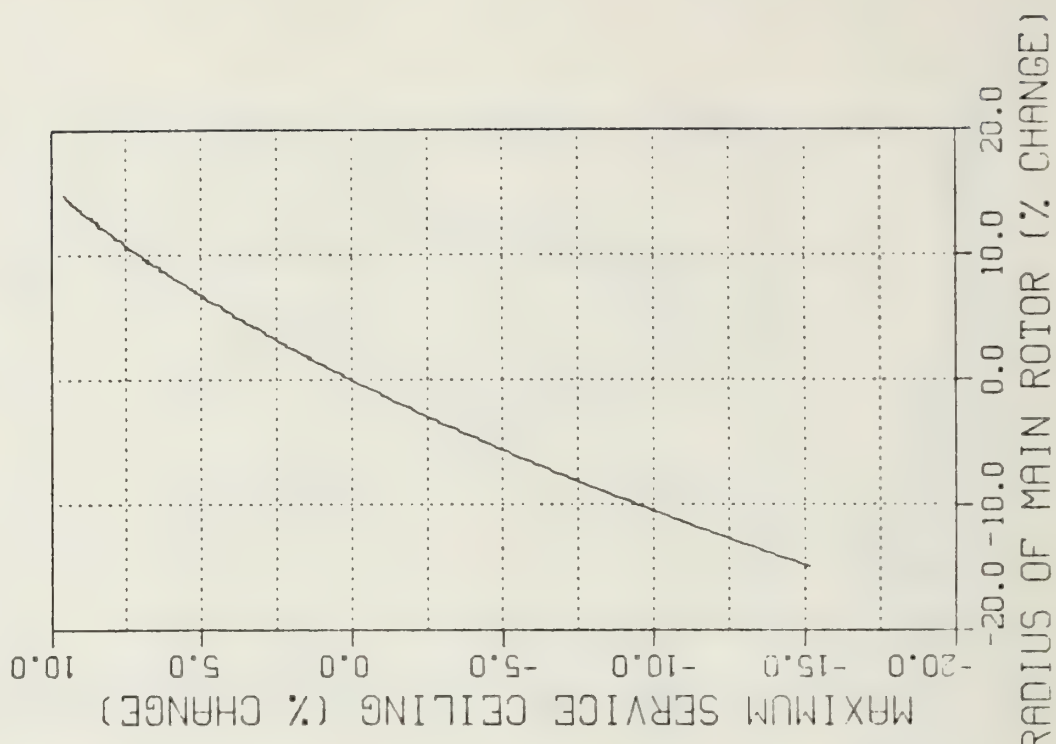
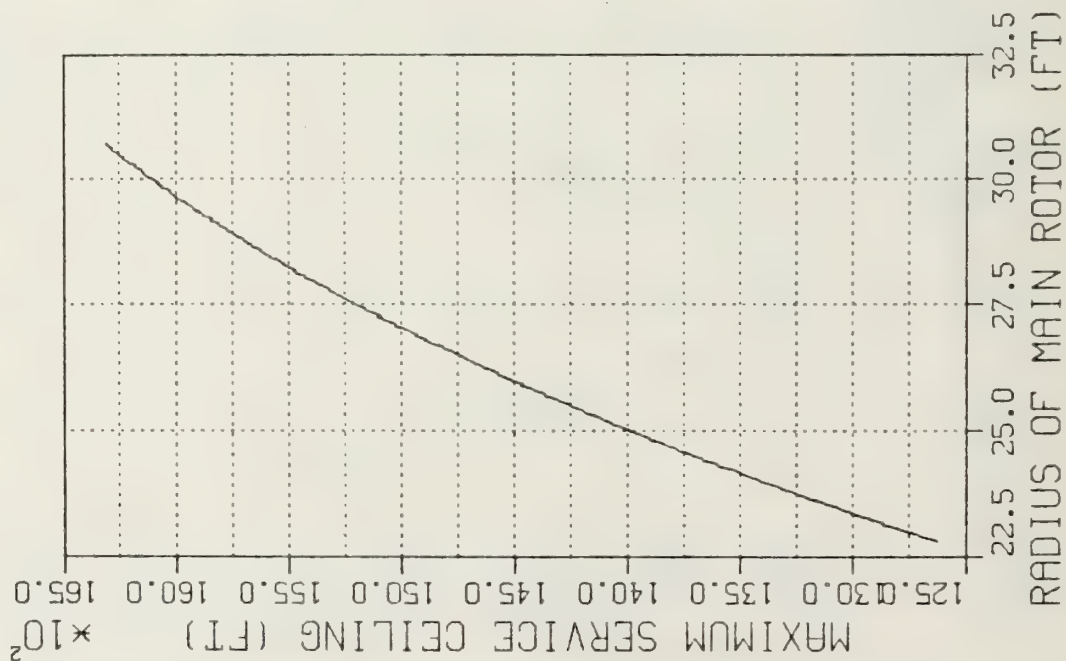
# MAXIMUM SERVICE CEILING VERSUS RADIUS CHANGE CHORD, TIP VELOCITY & ADVANCE RATIO HELD CONSTANT SOLIDITY, ROTATIONAL VELOCITY ALLOWED TO VARY WITH RADIUS



# MAXIMUM SERVICE CEILING VERSUS RADIUS CHANGE SOLIDITY & ROTATIONAL VELOCITY HELD CONSTANT CHORD, ADVANCE RATIO & TIP VELOCITY ALLOWED TO VARY WITH RADIUS



# MAXIMUM SERVICE CEILING VERSUS RADIUS CHANGE SOLIDITY, ADVANCE RATIO & TIP VELOCITY HELD CONSTANT CHORD & ROTATIONAL VELOCITY ALLOWED TO VARY WITH RADIUS













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PER01450
PER01460
PER01470
PER01480
PER01490
PER01500
PER01510
PER01520
PER01530
PER01540
PER01550
PER01560
PER01570
PER01580
PER01590
PER01600
PER01610
PER01620
PER01630
PER01640
PER01650
PER01660
PER01670
PER01680
PER01690
PER01700
PER01710
PER01720
PER01730
PER01740
PER01750
PER01760
PER01770
PER01780
PER01790
PER01800
PER01810
PER01820
PER01830
PER01840
PER01850
PER01860
PER01870
PER01880
PER01890
PER01900
PER01910
PER01920

WRITE(5,6001)
WRITE(5,6002)
WRITE(5,6003)
WRITE(5,6004)
WRITE(5,6005)
WRITE(5,6006)
WRITE(5,6007)
WRITE(5,6008)
WRITE(5,6009)
CALL RLINT(IANS)
CALL FRMTCMS('CLRSCRN',)
IF(IANS.EQ.3)OR(IANS.EQ.6)WRITE(5,6C10)
WRITE(5,6011)
FORMAT(10X,'YOU MAY CHOOSE ANY OF THE FOLLOWING PERFORMANCE')
FORMAT(10X,'FACTORS TO EXAMINE EACH ONE COULD TAKE 2-5 MINUTES')
FORMAT(10X,'TO RUN (ON AN AVERAGE),')
FORMAT(15X,'1. POWER REQUIREMENTS')
FORMAT(15X,'2. MAXIMUM ENDURANCE VELOCITY')
FORMAT(15X,'3. MAXIMUM RATE OF CLIMB')
FORMAT(15X,'4. MAXIMUM RANGE VELOCITY')
FORMAT(15X,'5. MAXIMUM HOVER CEILING (IGE)')
FORMAT(15X,'6. MAXIMUM SERVICE CEILING')
FORMAT(10X,'ENTER THE NUMBER (1,2,3,4,5,OR 6) YOU WISH TO EXAMINE')
*NE,
6010 FORMAT(5X,'THIS MAY TAKE SOME TIME IF THERE ARE ALOT OF USERS')
6011 FORMAT(5X,'CALCULATING RESULTS')
C*****
C# # # # # INPT DATA FOR HELICOPTER TO BE EXAMINED # # # # #
C*****
C----- INPUT MAIN ROTOR DATA -----
C----- RADIUS = 26.8 -----
C----- DIFF = 4.0 -----
C----- CMR1 = 1.75 -----
C----- RV MR1 = 27.0 -----
C----- CDCMR = 0.008 -----
C----- IBMR = 4 -----
C----- RTR = 5.5 -----
C----- CTR = 0.81 -----
C----- RVTR = 124.6 -----
C----- CDCCTR = 0.008 -----
C----- IBTR = 4 -----
C----- L = 31.5 -----
C----- W = 20000.0 -----

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EFPAF = 25.7
EFPVAV = 31.8
RTHT = 11.2
C----- INPUT ENGINE DATA -----
IENG = 2
SFCM = C.46
SFCN = C.47
SFCC = C.51
SHPM = 1561.0
SHPN = 1218.0
SHPC = 589.0
C----- INPUT FLIGHT VELOCITY FOR INITIAL POWER CALCULATIONS -----
VF1 = 90.0
C===== END OF REQUIRED INPUT INFORMATION =====
C=====
DO 3000 K = 1,4
VV1 = C.C
PA = 0.0
TEMP = C.0
DA = 0.0
DENSSL = 0.00237694
SKDHT = 2500.0
VF = VF1
VV = VV1
CMR = CMR1
RVMR = RVMR1
PIE = 3.141593
SDMR3 = 18MR*CMR1 / (PIE*RADIUS)
VTMR2 = RVMR1*RADIUS
CALL RHC
CALL RAC (DIFF, RADIUS, RRM, RMR, DRMR, MINZ, MAXZ, DMIN, DMAX)
IF (IANS .NE. 1) GO TO 2800
CALL PCWER
GO TO 3000
2800 IF (IANS .NE. 2) GO TO 2810
CALL ENCLUR
GO TO 3000
2810 IF (IANS .NE. 3) GO TO 2820
CALL ENCLUR
CALL MAXRC
GO TO 3000
2820 IF (IANS .NE. 4) GO TO 2830
CALL RANGE
GO TO 3000
2830 IF (IANS .NE. 5) GO TO 2840
CALL HCVER
GO TO 3000
2840 IF (IANS .NE. 6) GO TO 2850
GO TO 3000
PERO1530
PERO1540
PERO1550
PERO1560
PERO1570
PERO1580
PERO1590
PERO2000
PERO2010
PERO2020
PERO2030
PERO2040
PERO2050
PERO2060
PERO2070
PERO2080
PERO2090
PERO2100
PERO2110
PERO2120
PERO2130
PERO2140
PERO2150
PERO2160
PERO2170
PERO2180
PERO2190
PERO2200
PERO2210
PERO2220
PERO2230
PERO2240
PERO2250
PERO2260
PERO2270
PERO2280
PERO2290
PERO2300
PERO2310
PERO2320
PERO2330
PERO2340
PERO2350
PERO2360
PERO2370
PERO2380
PERO2390
PERO2400

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2850	CALL ENCLUR
	CALL CEILL
	GO TO 3000
3000	GO TO 5000
	CONTINUE
5000	CALL OCNEPL
	CONTINUE
	STCP
	END

[illegible]

SUBROUTINES USED IN PROGRAM FOLLOW

( )

SUPERQ1TINE\_RAD(DIFF,RADIUS,RRMR,RMR,DRMR,MINZ,MAXZ,DMIN,DMAX)

IMPLICIT REAL (A-H,L-Z)

DIMENSIONAL RMR (400), LRM (400)

RRMR = RADIALS - DIFF

$$10 \quad I = 1,324$$
$$\text{RMR}(I) = \text{RMR}$$

IF (I.EQ. 163) RMR(I) = RADIUS

$$RRMF = RMR + DIFF/162$$

TO CONTINUE

CONFIDENCE I = 1,324

$$DRMF(I) = ((RMR(I) - RMR(163)) / RMR(163)) * 100.0$$

20 DREF (I) - (KMK)  
CONTINUE

LINE = DMR (1)

DMAK = DRMR

UMAX	=	DIMK(5)
MIN7	=	BMR(1)

MIA X7  
MIA X7  
MIA X7  
MIA X7  
MIA X7

MAX 7 = RMK (324)

TURNER

三

[illegible]

SUB-GROUP B

# PERFORMANCE SUBROUTINES

[illegible][illegible]

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SUBROUTINE TO CALCULATE ALL PARTS OF THE TOTAL POWER REQUIREMENTS AND FIGURE OF MERIT.

AND FIGURE OF MERIT.

一、二、三、四、五、六、七、八、九、十、十一、十二、十三、十四、十五、十六、十七、十八、十九、二十、二十一、二十二、二十三、二十四、二十五、二十六、二十七、二十八、二十九、三十、三十一、三十二、三十三、三十四、三十五、三十六、三十七、三十八、三十九、四十、四十一、四十二、四十三、四十四、四十五、四十六、四十七、四十八、四十九、五十、五十一、五十二、五十三、五十四、五十五、五十六、五十七、五十八、五十九、六十、六十一、六十二、六十三、六十四、六十五、六十六、六十七、六十八、六十九、七十、七十一、七十二、七十三、七十四、七十五、七十六、七十七、七十八、七十九、八十、八十一、八十二、八十三、八十四、八十五、八十六、八十七、八十八、八十九、九十、九十一、九十二、九十三、九十四、九十五、九十六、九十七、九十八、九十九、一百。

[illegible]

SUPERROUTINE POWER

OVERDUTLINE POWER  
IMPLICIT REAL (A-H.1-7)

IMPLICIT REAL (A-H,I-Z)

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INTEGER I,J,K
COMMON /A/ AMR, ARMR, ARTR, ATR, CDOMR, CDOTR, CMR, CTMR, CTR, CTTR,
DA, DEN, EFAF, EFAV, GE, HD, LPA, RAD, ILCS, RIR, RIHT, RVMR, RVTR, SUMR,
SCIR, SKCHT, TEMP, W, VF, VV, IBTR, IBMR, DENSSL, PIE, PTMIN(400), VIMR,
VITR, VITR, VIMR, RANMAX, SFCC, SHPN, SHFN, SFFC, CMR1, RVMR1, RRM,
VTMR2, LIFF, SFCC, SHPN, SHFN, SFFC, CMR1, RVMR1, RRM,
CGMNCN /B/ PIMR(400), PCMR(400), PPMR(400), PTAC(400),
POTR(400), PTMR(400), PTTR(400), PTAC(400),
CCMNCN /C/ RMR(400), I, J, K, DRMR(400), MINX, MAXX, MINY, MAXY, MINZ,
MAXZ, CMIN, DMAX, MINB, MAXB, MINC, MAXC, MIN, MAX, MAXA, IANS, TEXT(200)
COMMON /H/ RCMAX(400), DRCMAX(400), VFRAN(400), DVFRAN(400),
HCVALT(400), DHOVAL(400), SEVALT(400), DSEVAL(400), FMERT(400),
DFMERT(400), VFEND(400), DVEND(400)
COMMON /Y/ DPIMR(400), DPMR(400), DPPMR(400), DPCMR(400), DPTMR(400),
DPITR(400), DPOTR(400), DPTAC(400), DPTTR(400)
C-----
MAX = 0.0
MAXA = C.0
DO 40 I = 1,324
CALL CONST
AMR = RMR(I)*2.0*PIE
IF(K .NE.1) GO TO 8
VTMR = VF / (RVMR*RM(1))
SCMR = IBMR / (PIE*RM(1))
IF(K .NE.2) GO TO 10
RVMR = VTMR2/RMR(1)
VTMR = RVMR*RM(1)
ARMR = VF / (RVMR*RM(1))
SCMR = IBMR / (PIE*RM(1))
IF(K .NE.3) GO TO 12
CMR = SDMR3*PIE*RM(1)/IBMR
RVMR = RVMR1
ARMR = VF / (RVMR*RM(1))
VTMR = RVMR*RM(1)
IF(K .NE.4) GO TO 14
CMR = SDMR3*PIE*RM(1)/IBMR
SCMR = IBMR*CMR / (PIE*RM(1))
VTMR = VTMR2/RMR(1)
ARMR = VF / (RVMR*RM(1))
CALL VELMR
CALL FCWMR
CALL VELTR
CALL FCWTR
IF(FIMR(I) .GT. MAXA) MAXA = PIMR(I)
IF(FCMR(I) .GT. MAXA) MAXA = PCMR(I)
PERO2E90
PERO2500
PERO2510
PERO2920
PERO2530
PERO2540
PERO2550
PERO2560
PERO2570
PERO2580
PERO2590
PERO3000
PERO3010
PERO3020
PERO3030
PERO3040
PERO3050
PERO3060
PERO3070
PERO3080
PERO3090
PERO3100
PERO3110
PERO3120
PERO3130
PERO3140
PERO3150
PERO3160
PERO3170
PERO3180
PERO3190
PERO3200
PERO3210
PERO3220
PERO3230
PERO3240
PERO3250
PERO3260
PERO3270
PERO3280
PERO3290
PERO3300
PERO3310
PERO3320
PERO3330
PERO3340
PERO3350
PERO3360

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      IF (FFMR(I) .GT. MAXA) MAXA = PPMR(I)
      IF (VV .LE. 0.0) GO TO 20
      IF (FCMR(I) .GT. MAXA) MAXA = PCMR(I)
      IF (PTAC(I) .GT. MAX) MAX = PTAC(I)
      VF = VF / 1.68885
      VV = VV * 60.0
20  CONTINUE
C-----
      MINY = 500.0
      MAXY = -500.0
      MINX = -500.0
      MAXX = 500.0
      DO 140 I = 1, 324
        DPIMR(I) = ((PCMR(I) - PPMR(163)) / PPMR(163)) * 100.0
        IF (DPIMR(I) .GT. MAXX) MAXX = DPIMR(I)
        IF (DPIMR(I) .LT. MINX) MINX = DPIMR(I)
        DPOMR(I) = ((POMR(I) - POMR(163)) / POMR(163)) * 100.0
        IF (DPOMR(I) .GT. MAXX) MAXX = DPOMR(I)
        IF (DPOMR(I) .LT. MINX) MINX = DPOMR(I)
        DPPMR(I) = ((PPMR(I) - PPMR(163)) / PPMR(163)) * 100.0
        IF (DPPMR(I) .GT. MAXX) MAXX = DPPMR(I)
        IF (DPPMR(I) .LT. MINX) MINX = DPPMR(I)
        IF (VV .LE. 0.0) GO TO 120
        DPCMR(I) = ((PCMR(I) - PCMR(163)) / PCMR(163)) * 100.0
        IF (DPCMR(I) .GT. MAXX) MAXX = DPCMR(I)
        IF (DPCMR(I) .LT. MINX) MINX = DPCMR(I)
        DPTMR(I) = ((PTMR(I) - PTMR(163)) / PTMR(163)) * 100.0
        DPTTR(I) = ((PTTR(I) - PTTR(163)) / PTTR(163)) * 100.0
        DPTTR(I) = ((PTTR(I) - PTTR(163)) / PTTR(163)) * 100.0
        DPTAC(I) = ((PTAC(I) - PTAC(163)) / PTAC(163)) * 100.0
        IF (DPTAC(I) .GT. MAXX) MAXX = DPTAC(I)
        IF (DPTMR(I) .GT. MAXX) MAXX = DPTMR(I)
        IF (DPTTR(I) .GT. MAXX) MAXX = DPTTR(I)
        IF (DPTAC(I) .LT. MINX) MINX = DPTAC(I)
        IF (DPTMR(I) .LT. MINX) MINX = DPTMR(I)
        IF (DPTTR(I) .LT. MINX) MINX = DPTTR(I)
120 CONTINUE
      CALL GRAF1C
      CALL GRAF1D
C-----
      VF = 0.0
      MINB = 1.0
      MAXB = 0.0
      DO 150 I = 1, 324
        CALL CCNST
        AMR = RMR(I) * 2.0 * PIE
        IF (K .NE. 1) GO TO 142
140 CONTINUE
      CALL GRAF1C
      CALL GRAF1D
C-----

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PER03370
PER03380
PER03390
PER03400
PER03410
PER03420
PER03430
PER03440
PER03450
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PER03470
PER03480
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PER03500
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PER03580
PER03590
PER03600
PER03610
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PER03630
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PER03660
PER03670
PER03680
PER03690
PER03700
PER03710
PER03720
PER03730
PER03740
PER03750
PER03760
PER03770
PER03780
PER03790
PER03800
PER03810
PER03820
PER03830
PER03840

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***      *      *      *
DA, DEN, EPPAF, EFPV, GE, HD, LPA, RADILS, RTR, RTHT, RVMR, RVTR, SCDM,
SCIR, SKCHT, TEMP, W, VF, VV, IBTR, IBMR, CENSSL, PIE, PTMIN(400), VIMR,
VITR, VITR, VIMR, RANMAX, THE TA, DELTA, SHPRAN(400), VV1, VF1, IENG, SDMR3,
VTMR2, CIFF, SFCC, SHPM, SHPN, SHFC, CMRI, RVMRI, RRM,
CCMMCN /B/, PIMR(400), POMR(400), PPMR(400), PCMR(400), PITR(400),
POTR(400), PTMR(400), PTR(400), PTAC(400)
CCMMON /C/ RM(400), I, J, K, DRMR(400), MINX, MAXX, MINY, MAY, MINZ,
MAXZ, DMIN, DMAX, MINB, MAXB, MINC, MAXC, MIN, MAX, MAXA, IANS, TEXT(200),
COMMON /W/ RCMA(400), DRCMA(400), VFRAN(400), DVFRAN(400),
HCVALT(400), DHQVAL(400), SEVALT(400), DSEVAL(400), FMERT(400),
DFMERT(400), VFEND(400), DVFEND(400)
CCMMON /Z/ VFEND1(400), VFEND2(400), VFEND3(400), VFEND4(400)
-----C-----
MAX = C.C
MIN = 500.0
CALL RHC
DO 280 I = 1, 324
AMR = RM(I)*#2 - 0*PIE
IF(K .NE. 1) GO TC 148
RVMR = RVMR + RM(I)
VIMR = VIMR + CMR / (PIE*RM(I))
SCMR = IBMR*CMR / (PIE*RM(I))
IF(K .NE. 2) GO TO 150
RVMR = VTMR2/RMR(I)
VIMR = RVMR*RM(I)
SCMR = IBMR*CMR1 / (PIE*RM(I))
IF(K .NE. 3) GO TO 152
CMR = SDMR3*PIE*RM(I)/IBMR
SCMR = IBMR*CMR / (PIE*RM(I))
RVMR = RVMR + RM(I)
VTMR = RVMR*RM(I)
IF(K .NE. 4) GO TO 154
CMR = SDMR3*PIE*RM(I)/IBMR
SCMR = IBMR*CMR / (PIE*RM(I))
RVMR = VTMR2/RMR(I)
VTMR = RVMR*RM(I)
PTMIN(I) = 10000.0
VFEND(I) = 0.0
CO 180 J = 1, 20
VF = FLOAT(J) * 10.0
CALL CONST
AMR = VF / (RVMR*RM(I))
CALL VELMR
CALL POWMR
CALL VELTR
CALL POWTR
IF (PTAC(I) .GT. PTMIN(I)) GO TO 160
PTMIN(I) = PTAC(I)

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160 VFEND(I) = VF/1.68885
180 CCNTINUE
CONTINUE
VFEND(I) = VFEND(I) - 10.0
VFF = VFEND(I)
DO 220 J = 1,20
VF = (FLOAT(J)-1.0) + VFF
CALL CONST
ARMR = VF / (RVMR*RRMR(I))
CALL VELMR
CALL POWMR
CALL VELTR
CALL POWTR
IF (PTAC(I) -GT. PTMIN(I)) GC TC 200
PTMIN(I) = PTAC(I)
VFEND(I) = VF/1.68889
CCNTINUE
200 CONTINUE
220 VFEND(I) = VFEND(I) - 1.0
VFF = VFEND(I)
DO 260 J = 1,200
VF = ((FLOAT(J)/100)-0.01) + VFF
CALL CONST
ARMR = VF / (RVMR*RRMR(I))
CALL VELMR
CALL POWMR
CALL VELTR
CALL POWTR
IF (PTAC(I) -GT. PTMIN(I)) GC TC 240
PTMIN(I) = PTAC(I)
VFEND(I) = VF/1.68889
CCNTINUE
240 CONTINUE
260 VFEND(I) = VFEND(I) - 0.01
IF(K.EQ.1) VFEND1(I) = VFEND(I)
IF(K.EQ.2) VFEND2(I) = VFEND(I)
IF(K.EQ.3) VFEND3(I) = VFEND(I)
IF(K.EQ.4) VFEND4(I) = VFEND(I)
IF(VFEND(I) .LT. MIN) MIN = VFEND(I)
IF(VFEND(I) .GT. MAX) MAX = VFEND(I)
CCNTINUE
280 MAXY = -500.0
MINY = 500.0
DO 480 I = 1,324
DVVFEND(I) = ((VFEND(I) - VFEND(163)) / VFEND(163)) * 100.0
IF(DVVFEND(I) .GT. MAXY) MAXY = DVVFEND(I)
IF(DVVFEND(I) .LT. MINY) MINY = DVVFEND(I)
CCNTINUE

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PER04810
PER04820
PER04830
PER04840
PER04850
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PER04870
PER04880
PER04890
PER04900
PER04910
PER04920
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PER04940
PER04950
PER04960
PER04970
PER04980
PER04990
PER05000
PER05010
PER05020
PER05030
PER05040
PER05050
PER05060
PER05070
PER05080
PER05090
PER05100
PER05110
PER05120
PER05130
PER05140
PER05150
PER05160
PER05170
PER05180
PER05190
PER05200
PER05210
PER05220
PER05230
PER05240
PER05250
PER05260
PER05270
PER05280

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492      IF(K .NE. 3) GO TO 494
          VF = VFEND3(I)
          CMR = SDMR3*PIE*RMR(I)/IBMR
          SCMR = IBMR*CMR/(PIE*RMR(I))
          VTMR = RVMR1*RMR(I)
494      IF(K .NE. 4) GO TO 496
          VF = VFEND4(I)
          CMR = SDMR3*PIE*RMR(I)/IBMR
          SCMR = IBMR*CMR/(PIE*RMR(I))
          VTMR = RVMR2*RMR(I)
496      DO 500 J = 1,80
          VV = FLOAT(J)*100.0
          CALL CONST
          ARMR = VF / (RVMR*RMR(I))
          CALL VELMR
          CALL POWMR
          CALL VELTR
          CALL POWTR
          IF (PTAC(I) .GT. PTAVAL) GO TO 520
          VF = VF/1.68889
          CONTINUE
500      RCMAXX = (VV*60.0) - 100.0
520      VF = VF/1.68889
          DO 540 J = 1,100
          VV = FLOAT(J)*1.0 + RCMAXX
          CALL CONST
          ARMR = VF / (RVMR*RMR(I))
          CALL VELMR
          CALL POWMR
          CALL VELTR
          CALL POWTR
          IF (PTAC(I) .GT. PTAVAL) GO TO 560
          VF = VF/1.68889
          CONTINUE
540      RCMAX(I) = (VV*60.0)-1.0
560      IF(RCMAX(I) .LT. MIN) MIN = RCMAX(I)
          IF(RCMAX(I) .GT. MAX) MAX = RCMAX(I)
          CONTINUE
580      C-----
          MAXY = -500.0
          MINY = 500.0
          DO 700 I = 1,324
          DRCMAX(I) = ((RCMAX(I) - RCMAX(163)) / RCMAX(163)) * 100.0
          IF (DRCMAX(I) .GT. MAXY) MAXY = DRCMAX(I)
          IF (DRCMAX(I) .LT. MINY) MINY = DRCMAX(I)
          CONTINUE
700      CALL GRAF3

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PERO5770
PERO5780
PERO5790
PERO5800
PERO5810
PERO5820
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PERO5840
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PERO5860
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PERO5880
PERO5890
PERO5900
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PERO5960
PERO5970
PERO5980
PERO5990
PERO6000
PERO6010
PERO6020
PERO6030
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PERO6070
PERO6080
PERO6090
PERO6100
PERO6110
PERO6120
PERO6130
PERO6140
PERO6150
PERO6160
PERO6170
PERO6180
PERO6190
PERO6200
PERO6210
PERO6220
PERO6230
PERO6240

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734	VTMR = RVMR1*RM(R(I))	PER06730
	IF(K.NE.4) GO TO 736	PER06740
	CMR = S DMR3*PIE*RM(R(I))/IBMR	PER06750
	RM(R) = IBMR*CMR / (PIE*RM(R(I)))	PER06760
	VTMR = RVMR2*RM(R(I))	PER06770
736	VTMR = RVMR*RM(R(I))	PER06780
	DO 740 J = 1,20	PER06790
	VF = FLOAT(J)*10.0	PER06800
	CALL CONST	PER06810
	ARMR = VF / (RVMR*RM(R(I)))	PER06820
	CALL VELMR	PER06830
	CALL POWMR	PER06840
	CALL VELTR	PER06850
	CALL POWTR	PER06860
	DE = 550.0*(PTAC(I)+PSHP) / VF	PER06870
	WDE = W / DE	PER06880
	IF (WDE.LE.RANMAX) GO TO 750	PER06890
	RANMAX = WDE	PER06900
	VFRAN(I) = VF/1.68889	PER06910
740	CONTINUE	PER06920
750	CONTINUE	PER06930
	VFF = VFRAN(I)	PER06940
	RANMAX = 0.0	PER06950
	DO 820 J = 1,20	PER06960
	VF = FLOAT(J)-1.0 + VFF	PER06970
	CALL CONST	PER06980
	ARMR = VF / (RVMR*RM(R(I)))	PER06990
	CALL VELMR	PER07000
	CALL POWMR	PER07010
	CALL VELTR	PER07020
	CALL POWTR	PER07030
	DE = 550.0 * (PTAC(I)+PSHP) / VF	PER07040
	IF (DE.EQ.0.0) GO TO 780	PER07050
	WDE = W / DE	PER07060
	GO TO 800	PER07070
	WDE = 0.0	PER07080
780	IF (WDE.LT.RANMAX) GO TO 850	PER07090
800	RANMAX = WDE	PER07100
	VFRAN(I) = VF/1.68889	PER07110
	CONTINUE	PER07120
820	CONTINUE	PER07130
850	VFF = VFRAN(I)	PER07140
	RANMAX = 0.0	PER07150
	DO 860 J = 1,201	PER07160
	VF = (FLCAT(J-1)/100.0) + VFF	PER07170
	CALL CONST	PER07180
	ARMR = VF / (RVMR*RM(R(I)))	PER07190
	CALL VELMR	PER07200





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COMMON /W/ RCMAX(400), DRCMAX(400), VFRAN(400), DVFRAN(400),
* HCVALT(400), DHOVAL(400), SEVALT(400), DSEVAL(400), FMERT(400),
* DMERT(400), VFEND(400), DVFEND(400)
C-----
VF = 0.C
VV = 0.C
SKCHT = 10.0
MIN = 3000.0
MAX = 0.0
PA = 0.0
TEMP = 0.0
IF (IENG .EQ. 1) PTAVAL = (FLOAT(IENG)*SHPN - 10.0) * 0.97
IF (IENG .EQ. 2) PTAVAL = (FLOAT(IENG)*SHPN - 10.0) * 0.9 * 0.97
IF (IENG .EQ. 3) PTAVAL = (FLOAT(IENG)*SHPN - 10.0) * 0.9 * 0.94
DO 1240 I = 1, 324
  AMR(I) = RMR(I)**2.0*PIE
  IF (K .NE. 1) GO TO 1108
  VIMR = RVMR1*RMR(I)
  SDMR = IBMR*CMR1 / (PIE*RMR(I))
1108 IF (K .NE. 2) GO TO 1112
  VIMR = VTMR2/RMR(I)
  SDMR = IBMR*CMR1 / (PIE*RMR(I))
1112 IF (K .NE. 3) GO TO 1114
  VIMR = RVMR3*PIE*RMR(I)/IBMR
  SDMR = IBMR*CMR / (PIE*RMR(I))
1114 IF (K .NE. 4) GO TO 1116
  VIMR = RVMR1*RMR(I)
  SDMR = SDMR3*PIE*RMR(I)/IBMR
  FVIMR = IBMR*CMR / (PIE*RMR(I))
  VIMR = VF / (RVMR*RMR(I))
1116 ARMR = VF / (RVMR*RMR(I))
DO 1120 J = 1, 30
  LA = FLOAT(J)*1000.0
  CALL RHO
  CALL CUNST
  CALL VELMR
  CALL POWMR
  CALL VELTR
  CALL POWTR
  FGWAA = PTAVAL*DELTA*SQRT(THETA)
  IF (PTAC(I) .LT. POWAA) GOTC 1120
  HCVALT(I) = LA
  GC TO 1140
  CCNT INUE
CONTINUE
HOV = HOVALT(I) - 1000.0
PER07690
PER07700
PER07710
PER07720
PER07730
PER07740
PER07750
PER07760
PER07770
PER07780
PER07790
PER07800
PER07810
PER07820
PER07830
PER07840
PER07850
PER07860
PER07870
PER07880
PER07890
PER07900
PER07910
PER07920
PER07930
PER07940
PER07950
PER07960
PER07970
PER07980
PER07990
PER08000
PER08010
PER08020
PER08030
PER08040
PER08050
PER08060
PER08070
PER08080
PER08090
PER08100
PER08110
PER08120
PER08130
PER08140
PER08150
PER08160

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1160 DO 1160 J = 1,20
1180   LA = FLOAT(J)*50.0 + HOV
      CALL RHO
      CALL CONST
      CALL VELMR
      CALL POWMR
      CALL VELTR
      CALL POWTR
      PCWAA = PTAVAL*DELTA*SQRT(THETA)
      IF (PTAC(I) .LT. POWAA) GOTC 1160
      HOVALT(I) = DA
      GC TO 1180
      CCNTINUE
1180 CONTINUE
      HOV = HOVALT(I) - 50.0
      DO 1200 J = 1,100
      LA = FLOAT(J)*0.5 + HOV
      CALL RHO
      CALL CONST
      CALL VELMR
      CALL POWMR
      CALL VELTR
      CALL POWTR
      PCWAA = PTAVAL*DELTA*SQRT(THETA)
      IF (PTAC(I) .LT. POWAA) GOTC 1200
      HOVALT(I) = DA-0.5
      GC TO 1220
      CCNTINUE
1200 CONTINUE
1220 IF (HOVALT(I) .LT. MIN) MIN = HOVALT(I)
      IF (HOVALT(I) .GT. MAX) MAX = HOVALT(I)
      CONTINUE
1240 C-----
      MAXY = -500.0
      MINY = 500.0
      DO 1400 I = 1,324
      DHOVAL(I) = ((HOVALT(I) - HOVALT(163)) / HOVALT(163)) * 100.0
      IF (CHOVAL(I) .GT. MAXY) MAXY = DHOVAL(I)
      IF (CHOVAL(I) .LT. MINY) MINY = CHOVAL(I)
      CONTINUE
1400 CALL GRAF5
      RETURN
      ENC
C*****
C SUBROUTINE TO CALCULATE THE MAXIMUM SERVICE CEILING
C*****
C*****

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PER08170
PER08180
PER08190
PER08200
PER08210
PER08220
PER08230
PER08240
PER08250
PER08260
PER08270
PER08280
PER08290
PER08300
PER08310
PER08320
PER08330
PER08340
PER08350
PER08360
PER08370
PER08380
PER08390
PER08400
PER08410
PER08420
PER08430
PER08440
PER08450
PER08460
PER08470
PER08480
PER08490
PER08500
PER08510
PER08520
PER08530
PER08540
PER08550
PER08560
PER08570
PER08580
PER08590
PER08600
PER08610
PER08620
PER08630
PER08640

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PER09130  
PER09140  
PER09150  
PER09160  
PER09170  
PER09180  
PER09190  
PER09200  
PER09210  
PER09220  
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PER09240  
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PER09260  
PER09270  
PER09280  
PER09290  
PER09300  
PER09310  
PER09320  
PER09330  
PER09340  
PER09350  
PER09360  
PER09370  
PER09380  
PER09390  
PER09400  
PER09410  
PER09420  
PER09430  
PER09440  
PER09450  
PER09460  
PER09470  
PER09480  
PER09490  
PER09500  
PER09510  
PER09520  
PER09530  
PER09540  
PER09550  
PER09560  
PER09570  
PER09580  
PER09590  
PER09600

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VF = VFF
CA = FLOAT(J)*1000.0
CALL RHO
VV = 100.0
CALL CONST / (RVMR*RM(R))
CALL VELMR
CALL POWMR
CALL VELTR
CALL POWTR
FCWAA = PTAVAL*DELTA*SQR(THETA)
IF (PTAC(I)) .LT. POWAA) GO TO 1420
IF (SEVALT(I)) = CA
GO TO 1440
CCNTINUE
CONTINUE
SEV = SEVALT(I) - 1000.0
DO 1460 J=1,20
VF = VFF
CA = FLOAT(J)*50.0 + SEV
CALL RHO
VV = 100.0
CALL CONST / (RVMR*RM(R))
CALL VELMR
CALL POWMR
CALL VELTR
CALL POWTR
FCWAA = PTAVAL*DELTA*SQR(THETA)
IF (PTAC(I)) .LT. POWAA) GO TO 1460
IF (SEVALT(I)) = CA
GO TO 1480
CCNTINUE
CONTINUE
SEV = SEVALT(I) - 50.0
DO 1500 J=1,100
VF = VFF
CA = FLOAT(J)*0.5 + SEV
CALL RHO
VV = 100.0
CALL CONST / (RVMR*RM(R))
CALL VELMR
CALL POWMR
CALL VELTR
CALL POWTR
FCWAA = PTAVAL*DELTA*SQR(THETA)
IF (PTAC(I)) .LT. POWAA) GO TO 1500

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1420  
1440

1460  
1480

















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CALL CPMCT (DRMR,DPTMR,322,0)
CALL CLURVE (DRMR,DPTAC,322,0)
CALL CLURVE (DRMR,DPTAC,322,0)
MAXLINE=LINEST(TEXT,100,30)
CALL HEIGHT(0.1)
CALL LINES(TAIL RCTOR POWER$,TEXT,1)
CALL LINES(MAIN ROTOR POWER$,TEXT,2)
CALL LINES(TOTAL POWER$,TEXT,3)
CALL LEGEND(TEXT,3,0.4,3.8)
CALL BLREC(0.3,3.7,1.55,0.75,1.2)
CALL RESET(HEIGHT)
CALL DCT
CALL GFIC (1,2)
CALL ENDGR(0)
-----
CALL PHYSOR(1.5,1.5)
CALL AREA2D(6.50,4.70)
CALL HEADIN (POWER VERSUS RADIUS$,19,1.4,3)
IF(K=NE.1) GO TO 8
CALL HEADIN (CHORD & ROTATIONAL VELOCITY HELD CONSTANT$,41,
*
CALL HEADIN (SOLIDITY, TIP VELOCITY & ADVANCE RATIO$,38,0.8,4)
CALL HEADIN (ALLOWED TO VARY WITH RADIUS$,27,0.8,4)
CALL MESSAGE (SPEC RMR=$,100,7.4,6.5)
CALL REALNO (RMR(163),2,ABUT,ABUT)
CALL MESSAGE (CASE 1$,100,8.7,6.0)
IF(K=NE.2) GO TO 10
CALL HEADIN (CHORD,TIP VELOCITY & ADVANCE RATIO HELD CONSTANT$,
*
CALL HEADIN (SOLIDITY, ROTATIONAL VELOCITY$,29,0.8,4)
CALL HEADIN (ALLOWED TO VARY WITH RADIUS$,27,0.8,4)
CALL MESSAGE (SPEC RMR=$,100,7.4,6.5)
CALL REALNO (RMR(163),2,ABUT,ABUT)
CALL MESSAGE (CASE 2$,100,8.7,6.0)
IF(K=NE.3) GO TO 12
CALL HEADIN (SOLIDITY & ROTATIONAL VELOCITY HELD CONSTANT$,
*
CALL HEADIN (CHORD, ADVANCE RATIO & TIP VELOCITY$,34,0.8,4)
CALL HEADIN (ALLOWED TO VARY WITH RADIUS$,27,0.8,4)
CALL MESSAGE (SPEC RMR=$,100,7.4,6.5)
CALL REALNO (RMR(163),2,ABUT,ABUT)
CALL MESSAGE (CASE 3$,100,8.7,6.0)
IF(K=NE.4) GO TO 14
CALL HEADIN (SOLIDITY, ADVANCE RATIO & TIP VELOCITY HELD CONSTANT$,
*
CALL HEADIN (CHORD & ROTATIONAL VELOCITY$,27,0.8,4)
CALL HEADIN (ALLOWED TO VARY WITH RADIUS$,27,0.8,4)

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PER12010  
 PER12020  
 PER12030  
 PER12040  
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 PER12060  
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 PER12280  
 PER12290  
 PER12300  
 PER12310  
 PER12320  
 PER12330  
 PER12340  
 PER12350  
 PER12360  
 PER12370  
 PER12380  
 PER12390  
 PER12400  
 PER12410  
 PER12420  
 PER12430  
 PER12440  
 PER12450  
 PER12460  
 PER12470  
 PER12480





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CALL BLREC(0.3,3.42,2.15,1.00,1.1)
CALL RESET('HEIGHT',)
CALL DCT
CALL GRID(1,2)
CALL ENDCR(0)

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-----
CALL PHYSOR(5.5,1.5)
CALL AREA2D(2.50,4.50)
CALL XNAME('RADIUS OF MAIN ROTCR (% CHANGE)',100)
CALL YNAME('POWER REQUIRED (% CHANGE)',100)
CALL GRAF(EMIN,SCALE,DMAX,MINX,SCALE,MAXX)
CALL LEGLIN
CALL CUFVE(DRMR,DPIMR,324,0)
CALL DASH
CALL CUFVE(DRMR,DPOMR,324,0)
CALL CFCNOT(DRMR,DPPMR,324,0)
CALL CFCVSH(DRMR,DPIR,324,0)
CALL DCT
CALL CUFVE(DRMR,DPCIR,324,0)
IF(V.LE.0.0) GOTO 22
CALL CUFVE(DRMR,DPCMR,322,0)
MAXLIN=LINEST(TEXT,100,30)
CALL HEIGHT(0.1)
CALL LINES('INDUCED POWER (MR)',TEXT,1)
CALL LINES('PROFILE POWER (MR)',TEXT,2)
CALL LINES('PARASITE POWER (MR)',TEXT,3)
CALL LINES('INDUCED POWER (TR)',TEXT,4)
CALL LINES('PROFILE POWER (TR)',TEXT,5)
CALL LEGEND(TEXT,5,0.4,3.50)
CALL BLREC(0.3,3.42,2.15,1.00,1.2)
CALL RESET('HEIGHT',)
CALL DCT
CALL GRID(1,2)
CALL ENDCR(0)
-----
CALL PHYSOR(1.5,1.5)
CALL AREA2D(6.50,4.70)
CALL HEACIN('POWER VERSUS RADIUS',19,1.4,3)
IF(K.EQ.1) GOTO 8
CALL HEACIN('CHORD & ROTATIONAL VELOCITY HELD CONSTANT',41,
*
CALL HEACIN('SOLIDITY, TIP VELOCITY & ADVANCE RATIO',38,0.8,4)
CALL HEACIN('ALLOWED TC VARY WITH RADIUS',27,0.8,4)
CALL MESSAGE('SPEC RMR =',100,7.4,6.5)
CALL REALNO(RMR(163),2,'ABUT','ABUT')
CALL MESSAGE('CASE 1',100,8.7,6.0)

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PER12570
PER12580
PER12590
PER13000
PER13010
PER13020
PER13030
PER13040
PER13050
PER13060
PER13070
PER13080
PER13090
PER13100
PER13110
PER13120
PER13130
PER13140
PER13150
PER13160
PER13170
PER13180
PER13190
PER13200
PER13210
PER13220
PER13230
PER13240
PER13250
PER13260
PER13270
PER13280
PER13290
PER13300
PER13310
PER13320
PER13330
PER13340
PER13350
PER13360
PER13370
PER13380
PER13390
PER13400
PER13410
PER13420
PER13430
PER13440

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```

8      IF(K .NE. 2) GO TO 10
      CALL HEADIN(,CHORC,TIP VELOCITY & ADVANCE RATIO HELD CONSTANT$,
*      48,0.8,4)
      CALL HEADIN(,SOLICITY, ROTATIONAL VELOCITY$,29,0.8,4)
      CALL HEADIN(,ALLOWED TO VARY WITH RADIUS$,27,0.8,4)
      CALL MESSAGE(,SPEC RMR =$,100,7.4,6.5)
      CALL REALNC(,RMR(163),2,ABUT,ABUT)
      CALL MESSAGE(,CASE 2$,100,8.7,6.0)
      IF(K .NE. 3) GO TO 12
      CALL HEADIN(,SOLIDITY & ROTATIONAL VELOCITY HELD CONSTANT$,
*      44,0.8,4)
      CALL HEADIN(,CHORC, ADVANCE RATIO & TIP VELOCITY$,24,0.8,4)
      CALL HEADIN(,ALLOWED TO VARY WITH RADIUS$,27,0.8,4)
      CALL MESSAGE(,SPEC RMR =$,100,7.4,6.5)
      CALL REALNC(,RMR(163),2,ABUT,ABUT)
      CALL MESSAGE(,CASE 3$,100,8.7,6.0)
      IF(K .NE. 4) GO TO 14
      CALL HEADIN(,SOLIDITY, ADVANCE RATIO & TIP VELOCITY HELD CONSTANT$,
*      51,0.8,4)
      CALL HEADIN(,CHORC & ROTATIONAL VELOCITY$,27,0.8,4)
      CALL HEADIN(,ALLOWED TO VARY WITH RADIUS$,27,0.8,4)
      CALL MESSAGE(,SPEC RMR =$,100,7.4,6.5)
      CALL REALNC(,RMR(163),2,ABUT,ABUT)
      CALL MESSAGE(,CASE 4$,100,8.7,6.0)
      CALL ENCLPL(0)
      RETURN
      END
C*****
C      SUBROUTINE TO CREATE GRAPH FOR ENDURANCE VELOCITY VS RADIUS
C*****
C      SUBROUTINE GRAF2
      IMPLICIT REAL (A-H, I-Z)
      COMMON /C/ RMR(400), I, J, K, DRMR(400), MINX, MAXX, MINY, MAXY, MINZ,
*      MAXZ, CMIN, DMAX, MINB, MAXB, MINC, MAXC, MIN, MAX, MAXA, IANS, TEXT(200)
      COMMON /W/ RCMAX(400), DRCMAX(400), VFRAN(400), DVFRAN(400),
*      HCVALT(400), DHOVAL(400), SEVALT(400), DSEVAL(400), FMERT(400),
*      DFMERT(400), VFEND(400), DVFEND(400)
      CALL CCNPRS
      CALL PAGE(11,0,8.5)
      CALL PHYSOR(1,5,1.5)
      CALL AREA2C(2,50,4.50)
      CALL XNAME(,RADIUS OF
      CALL YNAME(,ENDURANCE VELOCITY (KNOTS)$,100)
      CALL GRAF(,MINZ,SCALE,MAXZ,MIN,SCALE,MAX)
      CALL CUFVE(,RMR,VFEND,324,0)

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CALL DCT	PERI 3530
CALL GRID (1,2)	PERI 3940
CALL RESET(.DOT.)	PERI 3550
CALL ENDGR(0)	PERI 3560
C-----	
CALL PHYSOR(5,5,1.5)	PERI 3580
CALL AREA2D (2.50,4.50)	PERI 3590
CALL XNAME (RADIUS OF MAIN ROTOR (% CHANGE)\$,100)	PERI 4000
CALL YNAME (ENDURANCE VELOCITY (\$,100)	PERI 4010
CALL GRAF (DMIN, SCALE, DMAX, MINY, SCALE, MAXY)	PERI 4020
CALL CURVE (DRMR, DVFEND, 324,0)	PERI 4030
CALL DCT	PERI 4040
CALL GRID (1,2)	PERI 4050
CALL ENDGR(0)	PERI 4060
C-----	
CALL PHYSOR(1.5,1.5)	PERI 4070
CALL AREA2D (6.50,4.70)	PERI 4080
CALL HEADIN (ENDURANCE VELOCITY VERSUS RADIUS\$,32,1.4,3)	PERI 4090
IF(K.NE.1) GO TO 8	PERI 4100
CALL HEADIN (.CHORD & ROTATIONAL VELOCITY HELD CONSTANT\$,41,	PERI 4110
0.8,3)	PERI 4120
* CALL HEADIN (.SOLIDITY, TIP VELOCITY & ADVANCE RATIO\$,38,0.8,4)	PERI 4130
CALL HEADIN (.ALLOWED TO VARY WITH RADIUS\$,27,0.8,4)	PERI 4140
CALL MESSAGE (.SPEC RMR=\$,100,7.4,6.5)	PERI 4150
CALL REALNO (RMR(1,63),2,ABUT\$,ABUT\$)	PERI 4160
CALL MESSAGE (.CASE 1\$,100,8.7,6.0)	PERI 4170
IF(K.NE.2) GO TO 10	PERI 4180
CALL HEADIN (.CHORD,TIP VELOCITY & ADVANCE RATIO HELD CCNSTANT\$,	PERI 4190
48,0.8,4)	PERI 4200
* CALL HEADIN (.SOLIDITY, ROTATIONAL VELOCITY\$,29,0.8,4)	PERI 4210
CALL HEADIN (.ALLOWED TO VARY WITH RADIUS\$,27,0.8,4)	PERI 4220
CALL MESSAGE (.SPEC RMR=\$,100,7.4,6.5)	PERI 4230
CALL REALNC (RMR(1,63),2,ABUT\$,ABUT\$)	PERI 4240
CALL MESSAGE (.CASE 2\$,100,8.7,6.0)	PERI 4250
IF(K.NE.3) GO TO 12	PERI 4260
CALL HEADIN (.SOLIDITY & ROTATIONAL VELOCITY HELD CONSTANT\$,	PERI 4270
44,0.8,4)	PERI 4280
* CALL HEADIN (.CHORD, ADVANCE RATIO & TIP VELOCITY\$,34,0.8,4)	PERI 4290
CALL HEADIN (.ALLOWED TO VARY WITH RADIUS\$,27,0.8,4)	PERI 4300
CALL MESSAGE (.SPEC RMR=\$,100,7.4,6.5)	PERI 4310
CALL REALNC (RMR(1,63),2,ABUT\$,ABUT\$)	PERI 4320
CALL MESSAGE (.CASE 3\$,100,8.7,6.0)	PERI 4330
IF(K.NE.4) GO TO 14	PERI 4340
CALL HEADIN (.SOLIDITY, ADVANCE RATIO & TIP VELOCITY HELD CCNSTANT\$,	PERI 4350
51,0.8,4)	PERI 4360
* CALL HEADIN (.CHORD & ROTATIONAL VELOCITY\$,27,0.8,4)	PERI 4370
CALL HEADIN (.ALLOWED TO VARY WITH RADIUS\$,27,0.8,4)	PERI 4380
CALL MESSAGE (.SPEC RMR=\$,100,7.4,6.5)	PERI 4390
CALL MESSAGE	PERI 4400









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CALL AREA2C (2.50,4.50)
CALL XNAME ('RADIUS OF MAIN ROTCR (FT) $',100)
CALL YNAME ('MAXIMUM RANGE VELOCITY (KNOTS) $',100)
CALL GRAF (MINZ,SCALE,MAXZ,MIN,SCALE,MAX)
CALL CLFVE (RMR,VFRAN,324,-1)
CALL DCT
CALL GRID (1,2)
CALL RESET ('DOT')
CALL ENGR(0)
*****
CALL PHYSOR(5.5,1.5)
CALL AREA2C (2.5,4.5)
CALL XNAME ('RADIUS OF MAIN ROTCR (% CHANGE) $',100)
CALL YNAME ('MAXIMUM RANGE VELOCITY (% CHANGE) $',100)
CALL GRAF (DMIN,SCALE,DMAX,MINY,SCALE,MAXY)
CALL CLFVE (DRMR,DVFRAN,324,-1)
CALL DCT
CALL GRID (1,2)
CALL ENGR(0)
-----
CALL PHYSOR(1.5,1.5)
CALL AREA2C (6.50,4.70)
CALL HEADIN ('MAXIMUM RANGE VELOCITY VERSUS RADIUS CHANGE $',
43,1.4,4)
* IF (K .NE. 1) GO TO 8
CALL HEADIN ('CHORD & ROTATIONAL VELOCITY HELD CONSTANT $',41,
0.8,3)
* CALL HEADIN ('SOLIDITY, TIP VELOCITY & ADVANCE RATIO $',38,0.8,4)
CALL HEADIN ('ALLOWED TO VARY WITH RADIUS $',27,0.8,4)
CALL MESSAGE ('SPEC RMR = $',100,7.4,6.5)
CALL REALNG ('RMR(1.63),2,ABUT,ABUT')
CALL MESSAGE ('CASE 1 $',100,8.7,6.0)
IF (K .NE. 2) GO TO 10
* CALL HEADIN ('CHORD,TIP VELOCITY & ADVANCE RATIO HELD CONSTANT $',
48,0.8,4)
CALL HEADIN ('SOLIDITY, ROTATIONAL VELOCITY $',29,0.8,4)
CALL HEADIN ('ALLOWED TO VARY WITH RADIUS $',27,0.8,4)
CALL MESSAGE ('SPEC RMR = $',100,7.4,6.5)
CALL REALNG ('RMR(1.63),2,ABUT,ABUT')
CALL MESSAGE ('CASE 2 $',100,8.7,6.0)
IF (K .NE. 3) GO TO 12
* CALL HEADIN ('SOLIDITY & ROTATIONAL VELOCITY HELD CONSTANT $',
44,0.8,4)
CALL HEADIN ('CHORD, ADVANCE RATIO & TIP VELOCITY $',34,0.8,4)
CALL HEADIN ('ALLOWED TO VARY WITH RADIUS $',27,0.8,4)
CALL MESSAGE ('SPEC RMR = $',100,7.4,6.5)
CALL REALNG ('RMR(1.63),2,ABUT,ABUT')
CALL MESSAGE ('CASE 3 $',100,8.7,6.0)

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8

10







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COMMON /W/ RCMAX(400), DRCMAX(400), VFRAN(400), DVFRAN(400),
* HCVALT(400), DHOVAL(400), SEVALT(400), DSEVAL(400), FMERT(400),
* DFMERT(400), VFEND(400), DVFEND(400),
CALL CCMPRS
CALL PACE(11,0,8.5)
CALL PHYSOR(1.5,1.5)
CALL AREA2D(2.50,4.50)
CALL XNAME('RADIUS OF MAIN ROTOR (FT)',100)
CALL YNAME('MAXIMUM SERVICE CEILING (FT)',100)
CALL GRAF(MINZ,SCALE,MAXZ,MIN,SCALE,MAX)
CALL CURVE(RMR,SEVALT,322,0)
CALL DCT
CALL GRID(1,2)
CALL RESET('DOT')
CALL ENGR(0)
-----C-----
CALL PHYSOR(5.5,1.5)
CALL AREA2D(2.50,4.50)
CALL XNAME('RADIUS OF MAIN ROTOR (% CHANGE)',100)
CALL YNAME('MAXIMUM SERVICE CEILING (% CHANGE)',100)
CALL GRAF(DMIN,SCALE,DMAX,MINY,SCALE,MAXY)
CALL CURVE(DRMR,DSEVAL,324,0)
CALL DCT
CALL GRID(1,2)
CALL ENGR(C)
-----C-----
CALL PHYSOR(1.5,1.5)
CALL AREA2D(6.50,4.70)
CALL HEADIN('MAXIMUM SERVICE CEILING VERSUS RADIUS CHANGES',
44,1.4,4)
* IF(K.NE.1) GO TO 8
CALL HEADIN('CHORD & ROTATIONAL VELOCITY HELD CONSTANT',41,
0.8,3)
* CALL HEADIN('SOLIDITY, TIP VELOCITY & ADVANCE RATIO',38,0.8,4)
CALL HEADIN('ALLOWED TO VARY WITH RADIUS',27,0.8,4)
CALL MESSAG('SPEC RMR =',100,7.4,6.5)
CALL REALNO(RMR(1.63),2,ABUT,ABUT)
CALL MESSAG('CASE 1',100,8.7,6.0)
IF(K.NE.2) GO TO 10
CALL HEADIN('CHORD, TIP VELOCITY & ADVANCE RATIO HELD CONSTANT',
48,0.8,4)
* CALL HEADIN('SOLIDITY, ROTATIONAL VELOCITY',29,0.8,4)
CALL HEADIN('ALLOWED TO VARY WITH RADIUS',27,0.8,4)
CALL MESSAG('SPEC RMR =',100,7.4,6.5)
CALL REALNO(RMR(1.63),2,ABUT,ABUT)
CALL MESSAG('CASE 2',100,8.7,6.0)
IF(K.NE.3) GO TO 12
CALL HEADIN('SOLIDITY & ROTATIONAL VELOCITY HELD CONSTANT',
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*      4, C.8, 4) CHORD, ADVANCE RATIO & TIP VELCCITY$, 34, 0.8, 4)
CALL HEADIN (, ALLOWED TO VARY WITH RADIUS$, 27, 0.8, 4)
CALL MESSAG (, SPEC RMR = $, 100, 7.4, 6.5)
CALL REALNO (RMR(163), 2, ABUT, , ABUT)
CALL MESSAG (, CASE 3$, 100, 8.7, 6.0)
IF ( K NE. 4) GO TO 14
CALL HEADIN (, SOLIDITY, ADVANCE RATIO & TIP VELOCITY HELD CONSTANT$,
*      51, 0.8, 4)
CALL HEADIN (, CHORD & ROTATIONAL VELCCITY$, 27, 0.8, 4)
CALL HEADIN (, ALLOWED TO VARY WITH RADIUS$, 27, 0.8, 4)
CALL MESSAG (, SPEC RMR = $, 100, 7.4, 6.5)
CALL REALNO (RMR(163), 2, ABUT, , ABUT)
CALL MESSAG (, CASE 4$, 100, 8.7, 6.0)
CALL ENDPL(0)
RETURN
END
C*****
C      SUBROUTINE TO CREATE GRAPH OF FIGURE OF MERIT VS RADIUS
C*****
C      SUBROUTINE GRAFLE
C      IMPLICIT REAL (A-H, L-Z)
C      *      CMAXZ, CMIN, CMAX, CMINE, MAXB, MINC, MAXC, MIN, MAX, MAXA, IANS, TEXT(200)
C      *      COMMON /W/ RCMAX(400), DRCMAX(400), VFRAN(400), DVFRAN(400),
C      *      *      HCVALT(400), DHOVAL(400), SEVALT(400), DSEVAL(400), FMERT(400),
C      *      *      DFMER(400), VFEND(400), DVFEND(400)
C      CALL CCMPRS
C      CALL PAGE(11.0, 8.5)
C      CALL PHYSOR(1.5, 1.5)
C      CALL AREA2D (2.50, 4.50)
C      CALL XNAME (, RADIUS OF
C      CALL YNAME (, FIGURE OF MERIT$, 100)
C      CALL GRAF (MINZ, SCALE, MAXZ, MINB, SCALE, MAXB)
C      CALL CURVE (RMR, FMERT, 324, 0)
C      CALL DCT
C      CALL GRID (1, 2)
C      CALL RESET (, DOT, )
C      CALL ENDCGR(0)
C-----
C      CALL PHYSOR(5.5, 1.5)
C      CALL AREA2D (2.50, 4.50)
C      CALL XNAME (, RADIUS OF
C      CALL YNAME (, FIGURE OF MERIT (%, CHANGE)$, 100)
C      CALL GRAF (CMIN, SCALE, DMAX, MINC, SCALE, MAXC)

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CALL CLFVE (DRMR,DFMERT,324,0)
CALL DCT
CALL GRIC (1,2)
CALL ENDGR(0)
-----C-----
CALL PHYSOR(1.5,1.5)
CALL AREA2C (6.50,4.70)
CALL HEACIN (,FIGURE CF MERIT VERSUS RADIUS CHANGE$,
36,1.4,4)
* IF(K.NE.1) GO TO 8
CALL HEACIN (,CHORD & ROTATIONAL VELOCITY HELD CONSTANT$,41,
0.8,3)
* CALL HEACIN (,SOLIDITY, TIP VELOCITY & ADVANCE RATIO$,38,0.8,4)
CALL MESSAG (,ALLOWED TO VARY WITH RADIUS$,27,0.8,4)
CALL MESSAG (,SPEC RMR =$,100,7.4,6.5)
CALL REALNC (RMR(163),2,ABUT,ABUT)
CALL MESSAG (,CASE 1$,100,8.7,6.0)
IF(K.NE.2) GO TO 10
CALL HEACIN (,CHORD,TIP VELOCITY & ADVANCE RATIO HELD CONSTANT$,
48,0.8,4)
* CALL HEACIN (,SOLIDITY, ROTATIONAL VELOCITY$,29,0.8,4)
CALL HEACIN (,ALLOWED TO VARY WITH RADIUS$,27,0.8,4)
CALL MESSAG (,SPEC RMR =$,100,7.4,6.5)
CALL REALNC (RMR(163),2,ABUT,ABUT)
CALL MESSAG (,CASE 2$,100,8.7,6.0)
IF(K.NE.3) GO TO 12
CALL HEACIN (,SOLIDITY & ROTATIONAL VELOCITY HELD CONSTANT$,
44,C.8,4)
* CALL HEACIN (,CHORD,ADVANCE RATIO & TIP VELOCITY$,34,0.8,4)
CALL HEACIN (,ALLOWED TO VARY WITH RADIUS$,27,0.8,4)
CALL MESSAG (,SPEC RMR =$,100,7.4,6.5)
CALL REALNC (RMR(163),2,ABUT,ABUT)
CALL MESSAG (,CASE 3$,100,8.7,6.0)
IF(K.NE.4) GO TO 14
CALL HEACIN (,SOLIDITY,ADVANCE RATIO & TIP VELOCITY HELD CONSTANT$,
51,0.8,4)
* CALL HEACIN (,CHORD & ROTATIONAL VELOCITY$,27,0.8,4)
CALL HEACIN (,ALLOWED TO VARY WITH RADIUS$,27,0.8,4)
CALL MESSAG (,SPEC RMR =$,100,7.4,6.5)
CALL REALNC (RMR(163),2,ABUT,ABUT)
CALL MESSAG (,CASE 4$,100,8.7,6.0)
CALL ENCLP(C)
RETURN
END
=====
C SUBROUTINE RDINT -- INTERACTIVELY READS AN INTEGER REPLY
C INTO A FORTRAN PROGRAM. IF THE USER INADVERTENTLY ENTERS AN IMPROPER=
C
PER17770
PER17780
PER17790
PER17800
PER17810
PER17820
PER17830
PER17840
PER17850
PER17860
PER17870
PER17880
PER17890
PER17900
PER17910
PER17920
PER17930
PER17940
PER17950
PER17960
PER17970
PER17980
PER17990
PER18000
PER18010
PER18020
PER18030
PER18040
PER18050
PER18060
PER18070
PER18080
PER18090
PER18100
PER18110
PER18120
PER18130
PER18140
PER18150
PER18160
PER18170
PER18180
PER18190
PER18200
PER18210
PER18220
PER18230
PER18240

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C DATA CHARACTER THE S/R ISSUES A WARNING AND ALLOWS A RECOVERY.
C=====
C SUBROUTINE RJOINT ( IANS)
C INTEGER CCOUNT
C-----
10 COUNT=C
CONTINUE
COUNT=CCOUNT+1
IF (COUNT.LT.3) GO TO 20
WRITE (5,60)
GO TO 50
20 CONTINUE
READ (5,*,END=40,ERR=40) IANS
IF (IANS) 40,40,30
30 CONTINUE
RETURN
40 REWIND 5
WRITE (5,70)
GO TO 10
50 CONTINUE
STOP
C-----
60 FORMAT (//,5X,49HPROGRAM TERMINATION - TWO IMPROPER DATA ENTRIES
1)
70 FORMAT (1X,56HWARNING: IMPROPER DATA ENTRY ENTER A POSITIVE INTEGER.)
END

```

```

=PER18250
PER18260
PER18270
PER18280
PER18290
PER18300
PER18310
PER18320
PER18330
PER18340
PER18350
PER18360
PER18370
PER18380
PER18390
PER18400
PER18410
PER18420
PER18430
PER18440
PER18450
PER18460
PER18470
PER18480
PER18490
PER18500
PER18510
PER18520

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## LIST OF REFERENCES

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209712

Thesis

A222

Adamcik

c.1

Preliminary helicop-  
ter design decision  
making based on flight  
performance factors.

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Preliminary helicop-  
ter design decision  
making based on flight  
performance factors.



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